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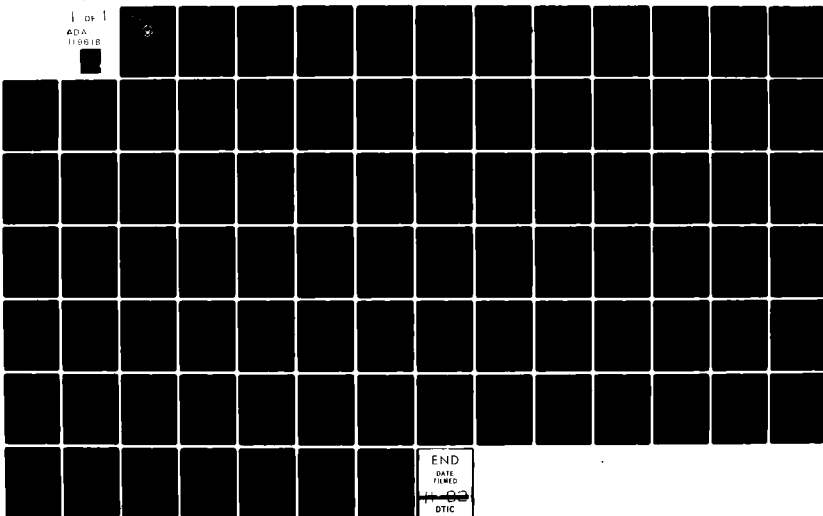
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## THESIS

AN ANALYSIS OF A PUFF DISPERSION  
MODEL FOR A COASTAL REGION

by

Stephen K. Rinard

June 1982

Thesis Advisor:

G. E. Schacher

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An Analysis of a Puff Dispersion Model for a Coastal Region

by

Stephen K. Rinard  
National Weather Service  
B.S., Texas A&M University, 1964

Submitted in partial fulfillment of the  
requirements for the degree of

MASTER OF SCIENCE IN METEOROLOGY

from the

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## ABSTRACT

The Risø National Laboratory, Roskilde, Denmark, atmospheric puff dispersion model has been tested for an atmospheric-marine environment. This three-dimensional model simulates the release of Gaussian pollutant puffs and predicts their concentration as they are diffused and advected downwind by a horizontally homogeneous, time-dependent wind. Atmospheric characteristics such as turbulence intensity, potential temperature gradient, buoyant heat flux and maximum mixing depth have been considered. Model predicted pollutant concentrations have been compared to airborne sampled observations. The effect of coastal turbulence not observed by the single point meteorological measurements made onboard ship greatly affects the advection and diffusion of a plume as it moves onshore. Additional measurements/predictions particular to the coastal area will have to be incorporated into the model for it to accurately predict the onshore movement of pollutants.

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## I. INTRODUCTION

The downwind transport and distribution of atmospheric pollutants from an isolated source over land or water has become an important environmental factor in today's society. The need to understand the distribution of smoke, unpleasant or potentially harmful foreign gases and perhaps radioactive debris from a nuclear powerplant accident are becoming more and more essential for industrial operations and construction planning. The dispersion of such atmospheric pollutants is commonly modeled by a standard Gaussian plume model which computes one-hour average plume characteristics.

The Meteorology Section of the Risø National Laboratory, Roskilde, Denmark, has recently developed a puff model for prediction and simulation of atmospheric pollutant diffusion. The model considers individual puffs of pollutants with specific release rates that are advected by a horizontally homogeneous wind over a grid. The wind input may be either the measured wind from a single point, a spatial average or a wind simulation. The model simulates the instantaneous plume characteristics by adding a group of puffs, growing in size, as they advect with the wind. A Gaussian plume model, on the other hand, provides a time

averaged concentration pattern based on a single time average wind vector. In the puff model, the plume advects with a time series of actual wind data. Thus, the puff model is able to predict time varying concentration distributions in actual changing wind conditions, making it an appropriate tool for dynamical computations of downwind dispersions of pollutants.

A basic comparison of a puff model simulation and a typical plume is illustrated in Fig. 1. Looking from above, the instantaneous behavior of a plume being advected from a source by the wind is shown. The outer cone-shaped contours represent the outer limit of the plume boundary and are identical in both Figs. 1 (A) and (B).

Fig. 1(A) shows an instantaneous depiction of an actual plume. The long-term average plume concentration is shown on the extreme right as a smooth curve with a maximum on the central axis. Also shown is the instantaneous plume concentration considered realistic but is of such a short time scale that it cannot be predicted or easily measured.

The puff model prediction is depicted in Fig. 1(B). The circles show the boundaries of individual puffs of pollutants released from the source. These puffs are advected

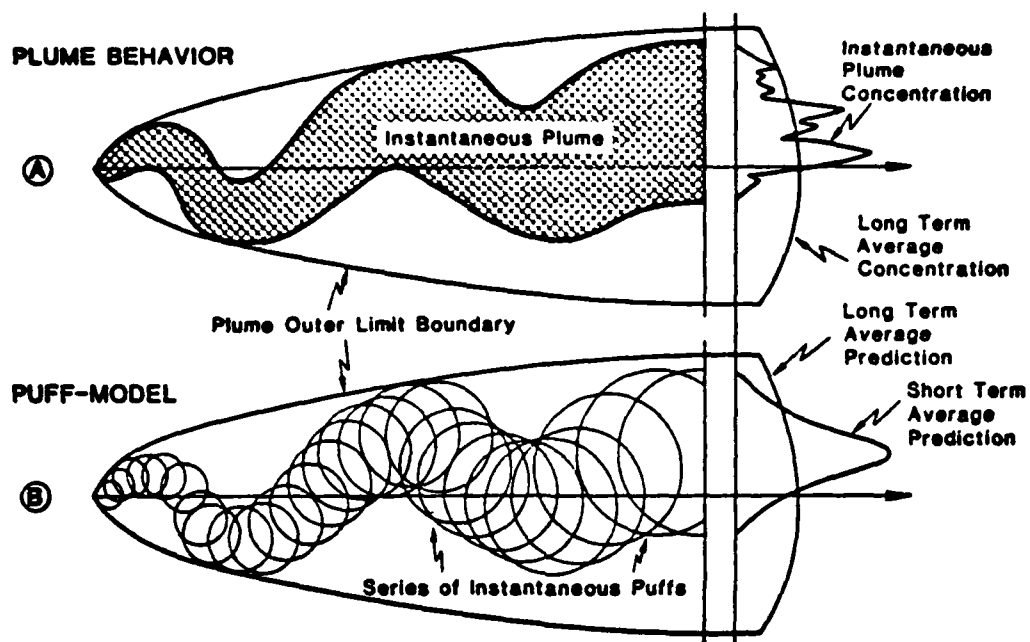


Figure 1. Instantaneous Behavior of a Typical Plume and a Series of Puffs from a Puff Model

and diffused downwind by a frequently updated wind. The long term average concentration prediction of the puff model is expected to be identical to the long term concentration of Fig. 1 (A). The short term average pollutant prediction, a Gaussian curve shown on the extreme right, is not completely realistic but is a reasonable approximation to the instantaneous plume concentration profile.

The purpose of this thesis is to evaluate and test the general characteristics and capabilities of the Risø puff model. The adjustable input data will be varied and predicted results for various input combinations compared. A preliminary comparison will also be made between predicted results and data collected from a coastal region using observed meteorological forcing data as model input.

## II. RISØ PUFF MODEL

### A. GENERAL CHARACTERISTICS

The Risø Puff Model is a three-dimensional computer model used for the prediction and/or simulation of the diffusion and advection of atmospheric pollutants. The puff model technique is to simulate a plume with Gaussian shaped puffs with specified release rates within a specified grid. The initial size of the puffs is normally one meter in diameter although this can be easily adjusted. The amount of material in a puff is the release rate times the elapsed time between puffs. Therefore, a long elapsed time between puff releases results in a higher initial puff pollutant concentration than a short time interval. This should not normally be of concern if an adequate balance is maintained between grid size, advection speed and puff release rate.

The location of the puffs on the grid is determined by computing their movement for a finite time step using a measured wind field. The growth and buoyancy of the puffs are computed from simultaneous specifications of atmospheric turbulence intensity and stability and from buoyant heat



flux at the source. An inversion cap through which pollutants cannot pass and the source height where pollutants are released are variable and can easily be adjusted. Grid distances within the model may vary from meters to kilometers and time durations from seconds to hours are possible.

This puff model has the capability of monitoring a maximum of twenty-five sources of puffs and its grid may contain up to 100 puffs. A puff source can be located anywhere on the grid and have a unique release rate, start and stop of release time, and heat production. When the center of a puff moves outside the boundaries of the grid (either horizontally or vertically), that particular puff is dropped from memory. In this way the model does not store irrelevant puff information, thus keeping computer memory requirements to a minimum.

A variable to control the amount of reflection/absorption of the pollutant by the surface is easily adjusted in the puff model. Such a parameter is of great value both in actual dispersion problems and also for gaining understandings of the plume/surface relationship.

The model calculates the concentration at each grid point by summing the contributions from surrounding puffs

for each advection step. The grid concentrations can be allowed to accumulate or simply be updated with the latest instantaneous value. A minimum grid concentration of interest can be set to reduce computer run time by dropping concentrations too small to be of interest.

The output of the model contains periodic results of puff locations and concentrations as well as initial input verification. The time interval for the periodic results is adjusted by the input data. This recurrent lineprinter output contains:

- X-Y plane plots showing the position of the sources and of puffs inside the grid,
- X-Z plane plots of puff positions for evaluating plume rise for each vertical level of interest, and
- a table listing of the grid point concentrations for each level.

A computer drawn contour chart of the magnitudes of the pollutant concentrations is also available.

When considering distance between gridpoints ( $\Delta X, Y, Z$ ), only spatial resolution and computer resources need be considered. Calculated concentration accuracy is not related to the grid-point separation. To insure that no essential information on individual puffs is "hidden" between grid points, the grid separation should be adjusted dependent upon the size of the puffs at the downwind distance of interest. Other specific model configuration considerations are described in the following sections. They are also discussed in more detail in the model behavior chapter.

#### B. WIND FIELD

Once a puff is released, it is advected based upon wind data measurements at a single point only, normally the release point. This limits the validity of the model to situations where the wind field and turbulence can be assumed to be horizontally homogeneous throughout the grid. It is therefore important to insure that the data obtained from such a single point measurement is representative of the wind structure for the whole area of interest.

The wind data are normally obtained in the form of a horizontal velocity time series. A vector sequence is formed

by averaging over a convenient interval. These data are read into the model after being segregated into turbulence classes as discussed in the next section.

### C. TURBULENCE INTENSITY AND DIFFUSION

The growth/diffusion of a puff depends upon the turbulence intensity. To account for this growth, the puff model applies the theory for relative diffusion suggested by Smith and Hay (1961).

The turbulence intensity is defined to be the standard deviation ( $\sigma$ ) of the wind direction (in radians) squared. The  $\sigma$  values are collected for the same short time periods as the wind speed measurements used to advect the puffs. Therefore, the intensity of the turbulence which governs the relative diffusion of the puffs, can be adjusted along with the the advecting wind speed after each time step, if conditions warrent.

A very low value of turbulence intensity (as 0.0002) represents a small standard deviation (0.9), normally a stable atmosphere and a weak puff dispersion/diffusion. As the atmosphere becomes more unstable, the turbulence intensity increases along with an increase of  $\sigma$  values and plume dispersion/diffusion. While these characteristics are

representative of turbulence over land, they can be applied to over water cases in a broad sense.

#### D. PLUME RISE

In the vertical direction, puff-rise can be accounted for by Briggs (1970) plume rise theory. In this case buoyancy is assumed to be conserved (adiabatic motion), and pressure forces, molecular viscosity and local density changes are considered small and are neglected. The rate at which a puff rises as it is advected downwind is a function of the buoyancy flux, wind speed, puff distance traveled and stability of the atmosphere. Plume rise is considered separately for each individual puff.

#### E. REFLECTION

The interaction of the pollutant with the surface is adjustable and can be easily changed in the input data. Total reflection or absorption or a fraction between the two can be used.

#### F. LIMIT OF MIXING DEPTH

The effect of an atmospheric lid (inversion) can be applied in the model to limit the vertical movement of the pollutant. The model does not permit the plume to rise

above this cap. When a maximum mixing level is in effect, it acts to totally reflect the pollutants in the same manner as total reflection at the surface. This mixing cap would act as an inversion when the puff would be expected to grow much more readily in the horizontal than in the vertical direction.

### III. DATA COLLECTION

An intensive field tracer study was performed during the fall of 1980 and winter of 1981 in the Santa Barbara Channel area of the California coast. The work was supported by the Bureau of Land Management (BLM) and performed by the Environmental Physics Group of the Naval Postgraduate School (NPS) and AeroVironment Inc (AV), Los Angeles, CA. This study was designed to help validate and/or modify Gaussian dispersion models for coastal use and to build a data base for future model development. Air pollution models in current use have not been adequately validated for the over-water regime.

In the experiment, a tracer gas ( $\text{SF}_6$ ) was released several miles offshore from the NPS Research Vessel (R/V) Acania. Ambient gas concentrations as low as 10 parts per trillion (PPT) were determined by an array of land based sensors, from a small boat and at various levels by an aircraft equipped with a continuous  $\text{SF}_6$  analyser. A chart of the experimental area and locations of the various platforms is shown in Fig. 2.

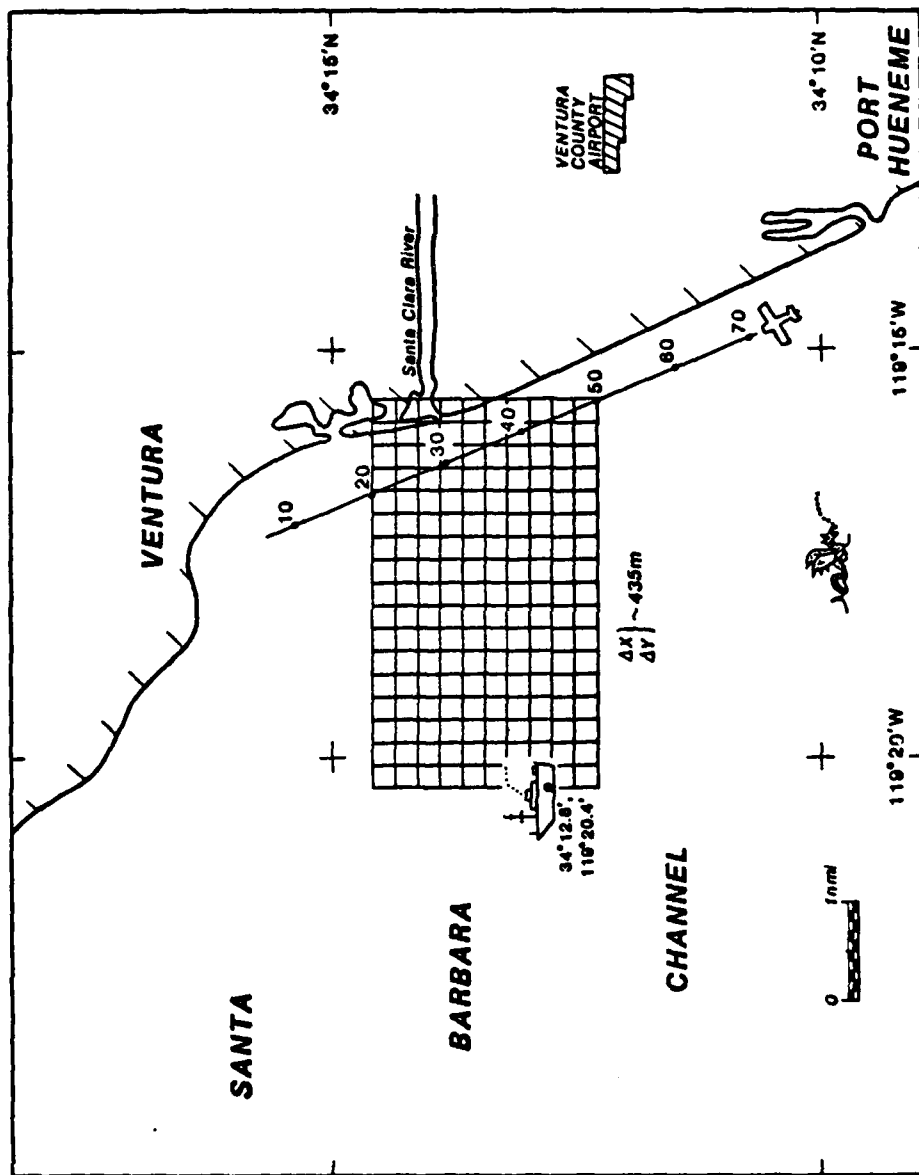


Figure 2. Experimental Area showing Locations of R/V Acacia, Aircraft track and Numerical Grid.



The aircraft flew through the plume at various elevations offshore and overland. The plume transect tracks pertinent to this study were made parallel to the coast approximately one-half mile offshore. The airborne sampling consisted of instantaneous concentrations (PPT) at selected points at different levels over a period of six hours. The observations, recorded at locations 10-70 at altitudes of 61 and 91 m above MSL on January 29, 1980 are shown in Fig. 3. Average concentrations over the noted time period are shown at the bottom of each altitude block.

The following marine meteorological parameters were measured onboard the R/V Acania while anchored approximately 7.4 km offshore:

- |   |                  |
|---|------------------|
| •relative wind speed                        | •air temperature |
| •wind speed fluctuation                     | •dew point       |
| •sea surface temperature                    | •ship roll       |
| •sky cloud cover                            | •ship location   |
| •relative wind direction                    |                  |
| •inversion height (acoustic sounder)        |                  |
| •vertical temperature and humidity profiles |                  |

(shipboard radiosonde launch every 12 hours).

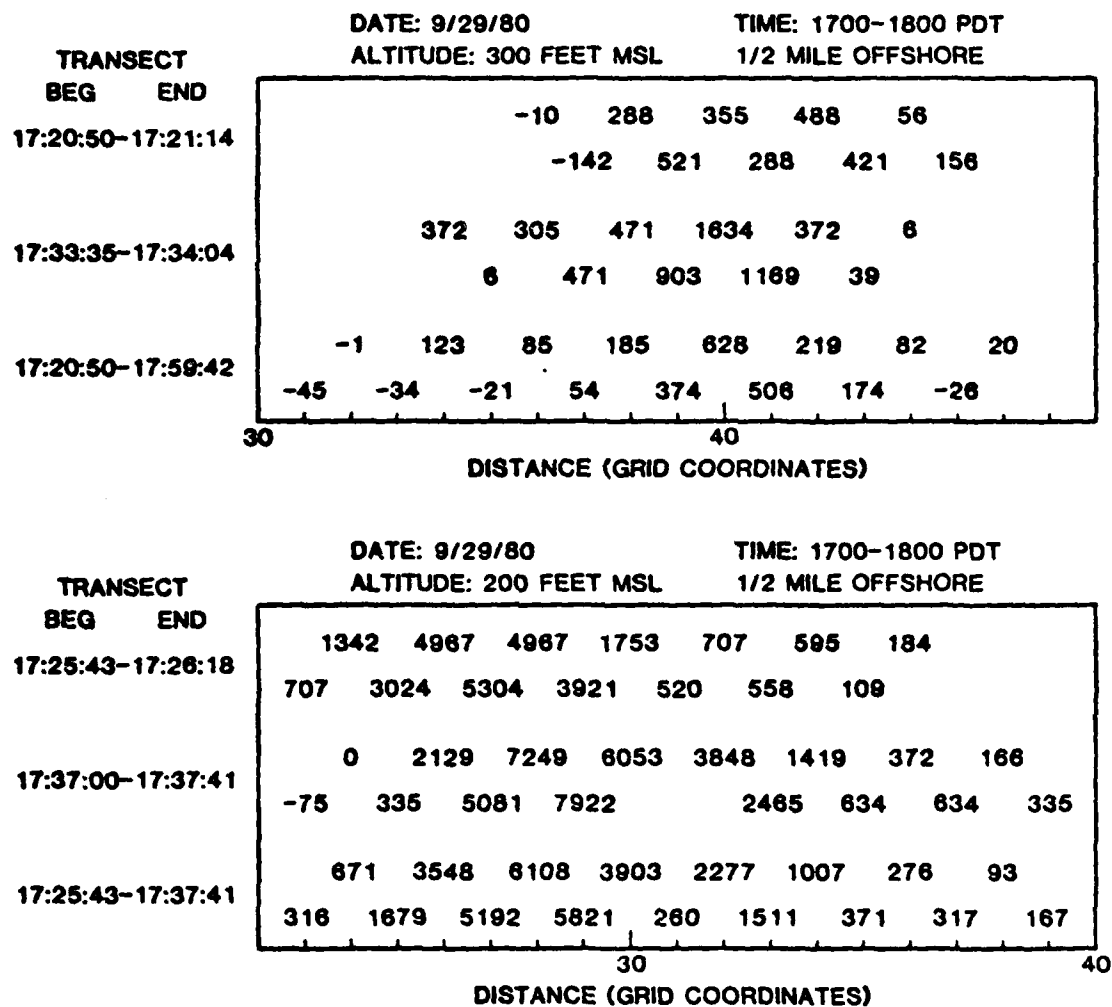


Figure 3. Aircraft observed Plume Concentrations (PPT) at Grid Coordinates at 61 and 91 m above MSL, 29 September 1980.

The tracer gas was released at a fixed rate through the exhaust of one of the ships motor generator sets. The generator was run at a constant speed resulting in a constant stack temperature and flow rate.

The above collected meteorological information enabled the data grid to be established and the atmospheric wind field, turbulence intensity, stability and buoyancy flux to be derived for inputs into the puff model. The puff model prediction based on this actual data formed the basis for the model performance evaluations carried out here. From this basis, different input variables were adjusted to note the effect on the advected concentrations--both in relation to each other and to the airborne measurements.

#### IV. MODEL BEHAVIOR

The Puff Model was run on the NPS IBM S/370 Model 3033 AP computer with two goals in mind; (1) familiarization with model performance under actual conditions and (2) a comparison of model predictions with observed data. The two goals are interrelated in the sense that atmospheric data collected in the aforementioned tracer study were used to form an initial prediction of the plume dispersion, and variations of that data were used to evaluate the limits of the model. The data used as input to the model represented the marine atmospheric conditions as determined from R/V Acania meteorological data at the time of the experiment.

Proper grid spacing was arrived at by considering puff spread, mean wind direction and the geographical area of interest. With the initial prediction in hand, data input variables of the model were adjusted and their effects (changes in prediction) noted. All model predictions were compared with the aircraft observed data.

A 7.4 X 4.3 km downwind area of interest was initially gridded into an 17 X 10 array. Distances between horizontal and vertical grid points were approximately 435 m (Fig. 2).

Since many of the aircraft observation times centered around 1730 hours (all times are Pacific Daylight Time), model puff releases were initiated at 1630. The 30-minute wind speed averages obtained from data taken onboard the ship between 1630 and 1730 were 4.7 and 4.8  $\text{ms}^{-1}$ . The first advected puffs would be expected to arrive at the back edge of the grid slightly before 1700, and by 1730 a steady consistent plume would be passing through the area of the aircraft track. (The model showed, in fact, puffs leaving the back edge of the grid slightly before 30 minutes after puff release).

The average wind direction was recorded on the ship every 15 seconds. The standard deviations of the wind direction ( $\sigma$ ) were computed as approximate one minute averages. These, in turn, were averaged over 30 minutes to correspond with the 30-minute wind speed averages. The  $\sigma$  values during the time of interest were 1.0 and 0.9 resulting in the very small turbulence intensity values of .0003 and .0002.

A delta Z value of 33 m was used to observe plume concentrations at the altitudes of 0, 33, 66 and 99 m above the surface. These levels were chosen for comparison with the aircraft transect altitudes of 61 and 91 m.

Fine scale vertical temperature and humidity plots were drawn based upon radiosonde soundings taken onboard the ship. The sounding taken at 1735 PDT (Figure 4) shows a shallow unstable layer near the surface topped by an inversion extending to near 400 m. A 80 m depth of the mixing layer was subjectively established. The potential temperature gradient computed by the formula

$$\frac{\partial \theta}{\partial z} = \frac{\partial T}{\partial z} + .0098 z \quad (1)$$

was found to be 1.0 deg K/100 m.

Basic data to determine source strength and heat emission from the ships stack were taken from Schacher, et al (1981). As previously mentioned,  $\text{SF}_6$  gas was released through the ships motor generator exhaust at a constant rate. The stack temperature was 250 deg F, the flow rate was  $7.13 \times 10^3 \text{ m}^3 \text{ s}^{-1}$ . The  $\text{SF}_6$  release rate was 47.91 lb  $\text{hr}^{-1}$ . The top of the ships stack--considered to be the source elevation-- was 4 m. The source strength was converted to  $6.04 \text{ gm s}^{-1}$  for input into the model.

Heat emission (H) in KW was determined by the formula

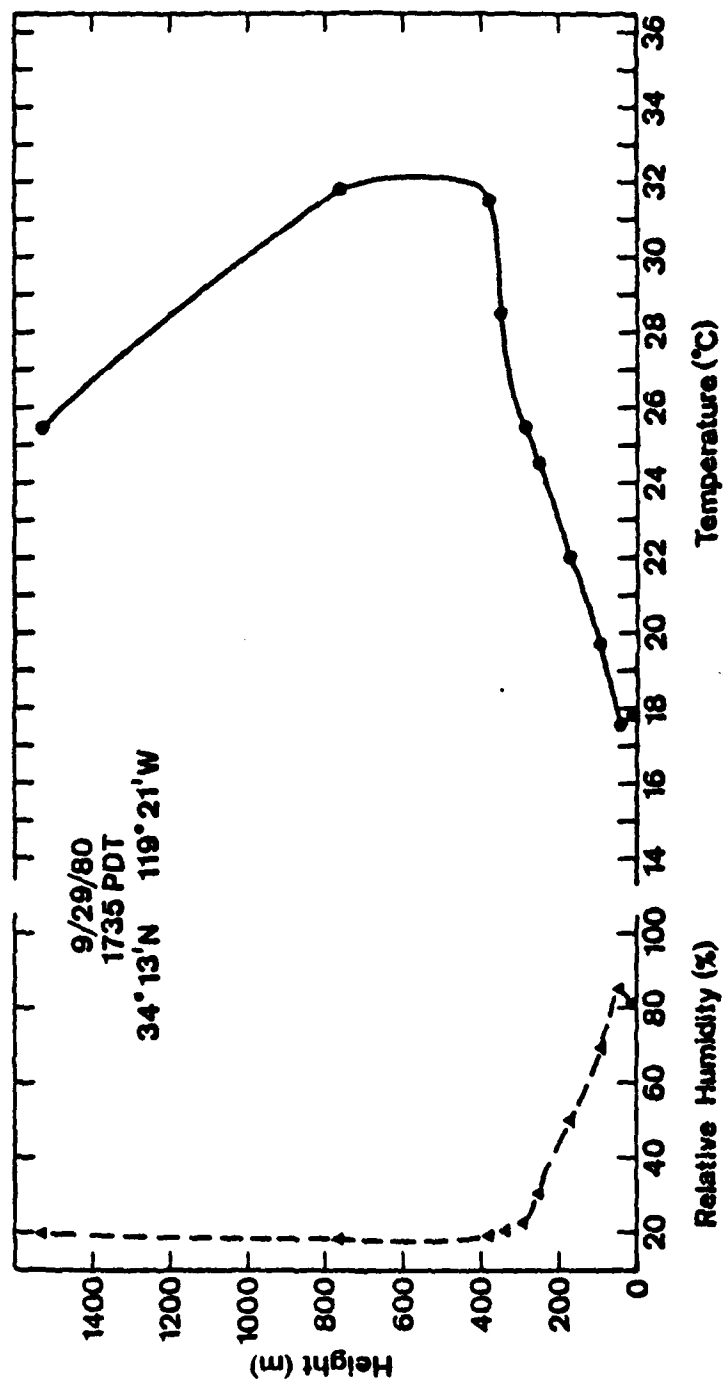


Figure 4. Radiosonde sounding taken onboard R/V Acania, 1745 PDT, September 29, 1981.

$$H = \Delta T * \frac{P}{RT} * C_p * \text{Flow} \quad (2)$$

where

delta T = temperature (stack - air) deg K

R = dry air gas constant

=  $2.87 \times 10^6$  erg/g deg K

P =  $10^3 * P(\text{mb})$  = dyne/cm<sup>2</sup>

C<sub>p</sub> = specific heat of dry air

= .24 cal/g deg K

Flow =  $16.39 * 7.13 * 10^3$  cm<sup>3</sup>/s

The heat emission was thus computed as 15.07 KW.

Initially the model grid was established after noting the area of maximum airborne sampled concentrations (between points 24 and 43 of Fig. 3) and the location of the ship. It became obvious during early model runs that, with the actual wind direction input, the model predicted plume was being advected south of the grid towards point 60 on the aircraft track. Obviously, the steering wind, as measured onboard ship, was not constant all the way to the shore. A northward turning of the plume was indeed detected several times during the experiments by the aircraft. To compensate



for this effect, the source of the plume release was moved in the model three grid spaces (1305 m) to the north so that the maximum predicted plume concentrations would pass through the areas of the maximum airborne measured concentrations. No corrections were made to the model predicted plume concentrations because of this adjustment. However, one could reason that the predicted concentration values would be higher in comparison with measured values since the coastal turbulence and wind shift--which would tend to diffuse the plume--were not considered.

Initial model runs with the small turbulence intensity classifications of .0003 and .0002 failed to show plume concentrations greater than  $1 \times 10^{-12}$  in the grid at any level other than at the source. Apparently, the grid spacing was too large and the narrow plume was advecting between the grid points. In an effort to locate the plume, a combination of model runs were performed varying the turbulence intensity and grid spacing as shown in Table I.

In this table, a mixing level cap of 80 m was in effect for the model predictions. No concentrations above that level were allowed in the computations. As previously mentioned, the model mixing level cap totally reflects all pollutants back downward.

TABLE I. A Comparison of Predicted Concentrations at the Surface, 40 and 80 m at the East Edge of the Grid with Turbulence Intensities between .01 and .05. Mixing Level Limit is 80 m. E = (\*10). Numbers in Parenthesis are Grid Numbers along Y Axis from Table II.

Turbulence Intensity	Delta Y	(4)	(5)	(6)	(7)	Sfc 40 m 80 m
.01	108.75	.68E-10 .31E-10 .47E-11	.16E-4 .70E-5 .11E-5	.22E-4 .10E-4 .15E-5	.20E-9 .91E-10 .14E-10	
.01	217.5	.69E-10 .31E-10 .47E-11		.22E-4 .10E-4 .15E-5		
.01	435	.69E-10 .31E-10 .47E-11				
.02	435	.19E-5 .17E-5 .12E-5				(7) .56E-8 .50E-8 .37E-8
.03	435	.66E-5 .67E-5 .62E-5				(7) .48E-6 .49E-6 .45E-6
.05	435	.57E-8 .59E-8 .58E-8	.72E-5 .74E-5 .72E-5			(7) .26E-5 .27E-5 .26E-5
						(8) .28E-9 .29E-9 .29E-9

With a grid spacing of 435 m and a turbulence intensity of .05, a plume concentration covering four grid spaces at the east end of the grid was produced. Predicted plume concentrations slowly decreased as the turbulence intensity was reduced to .02 (atmospheric stability increased). At an intensity of .01, the concentration dropped by about five orders of magnitude. Normally, one would expect increased concentrations with increased atmospheric stability. Perhaps the result noted here is due to the plume shrinking away from a grid point (and becoming more concentrated between the recorded grids) with the increase in stability.

To increase the grid resolution, the grid spacing was reduced by half to 217.5 m and again to 108.75 m. With each reduction the grid was reduced by half in the "Y" direction and doubled in the "X" direction thus keeping distances between grid spaces equal in all directions. This of course greatly increases the computational requirements. If only plume predictions along the back edge are needed (as in Table I), the downwind grid distance may be held constant at 435 m while the horizontal crosswind resolution is increased. In this way many unnecessary computations are not made. However, the increased horizontal crosswind resolution is

computed over the entire downwind grid, which in this case, is not necessary. A more satisfying solution to this problem is to install the capability of using a variable resolution grid with the model so that downwind areas of particular interest can be covered with a dense grid while other areas of not so much interest can be sparsely grided.

In order for the advection of the plume to remain on the array when increasing the horizontal crosswind resolution and decreasing the area exposed on the grid, the plume source was adjusted along the western boundary of the grid. The relationship of the vertical grid points to changes of the source location is shown in Table II. The plume source for each grid resolution is noted with an arrowhead. Grid points that are aligned vertically in the table have identical locations and should have the same predicted plume concentrations. As mentioned earlier, an increase of grid resolution does not affect the predicted concentration. Notice that for the same grid points in Table I, the predicted concentrations with a turbulence intensity of .01 remain constant with changes in grid spacing--only the grid resolution was changed.

TABLE II

The Relationship of the Y Axis along the Western Grid Edge to changes of Grid Distance between 435 and 108.75 m.

DELTA Y (m)	Grid Points Along the Y Axis											
435	4		5		6		7		8		9	
217.5	0	1	2	3	4	5	6	7	8	9		
108.75			0	1	2	3	4	5	6	7	8	9

From Table I it is obvious that the 435 m grid spacing is too large and that the higher resolution does indeed "see" concentrations that would otherwise be missed.

The problem of a increasingly narrow distance covered on the grid as resolution is increased can sometimes be at least partly corrected by reversing the X and Y coordinates and adjusting or rotating the advecting wind direction. This can easily be done with the use of the "TURN" model input parameter. This procedure sometimes becomes necessary since one of the grid directions is limited by the width of the output printer paper to less than or equal 10 grid units.

The model input variables, meteorological and source values were adjusted to note their effect on plume concentrations. A deeper understanding of how the model works and how the atmosphere affects dispersion can also be gained by

such adjustments. A turbulence intensity class of .05 was used, except when studying intensity itself, because it had previously demonstrated a good downwind grid coverage of the plume.

In order to note the effect of the maximum mixing level on the plume concentrations, several model predictions were run, varying only the height to which the plume was allowed to rise. Exact grid point reproductions were not possible since the model only allows the height of the mixing level to be an integer multiple of  $\Delta Z$ . The vertical grid spacing is therefore not equal. However, the anticipated trend of increased concentrations as the mixing level is lowered is evident from Table III.

The reflection/absorption of the plume at the surface is controlled by the model variable "REFLEC". Tests of the extremes of total absorption (0.0) and total reflection (1.0) were performed. The results showed a 50 percent reduction in plume concentrations at the west end of the grid with total absorption compared to total reflection in otherwise identical model runs.

The model has a self-imposed limitation of 100 puffs from all sources on the grid. The model will terminate if

TABLE III  
Plume Concentrations between Surface and 99 m under  
Different Maximum Mixing Levels.

Max Mixing Level	(5)	(6)	(7)	(8)	
None	.44E-8	.55E-5	.20E-5	.22E-9	Sfc
	.43E-8	.54E-5	.19E-5	.21E-9	33 m
	.40E-8	.50E-5	.18E-5	.20E-9	66 m
	.36E-8	.45E-5	.16E-5	.18E-9	99 m
80 m	.57E-8	.72E-5	.26E-5	.28E-9	Sfc
	.59E-8	.74E-5	.27E-5	.29E-9	40 m
	.58E-8	.72E-5	.26E-5	.29E-9	80 m
	0	0	0	0	> 80 m
30 m	.64E-8	.81E-5	.29E-5	.32E-9	Sfc
	.65E-8	.81E-5	.29E-5	.32E-9	30 m
	0	0	0	0	> 30 m

this number is exceeded. A balance must be made between the rate at which puffs are released from the source (TAU) and the time it takes the puffs to be advected across the grid. A release rate of one puff every 40 seconds was predominantly used during this study.

The turbulence intensity variable was varied to include conditions that are more unstable. As atmospheric instability increases, the plume would be expected to expand whereas, with stable conditions, the plume should remain narrow and highly concentrated.

With the use of NPS contouring routines and the subroutine "DRAW", a visual comparison of the plume disposition and concentrations is available. Since the computed plume concentration varies over many orders of magnitude, the concentration values were converted to integer numbers by multiplying by  $1. \times 10^{13}$  and then taking the logarithm. These logarithms are then smoothed. Thus, a contour plot representing order of magnitude concentrations was produced. As with the model variables "MAPTIM" and "KPLANS" which control the frequency and vertical levels of printer plots, "DRAW" can be called to contour concentrations at any time period and for any level required.

Plume concentration distributions for turbulence intensities of .05, .10 and .25, all other variables constant, are shown in Figs. 5, 6 and 7. As expected, the plume becomes wider and the concentration decreases as the turbulence intensity/diffusion increases and the atmosphere becomes less stable.

In Figs. 5-7, the plume source was located at grid point (0,6). The wide plume in the lower part of the plot is not real but is a function of the smoothing routine spreading the early puffs more than would be expected. Since the



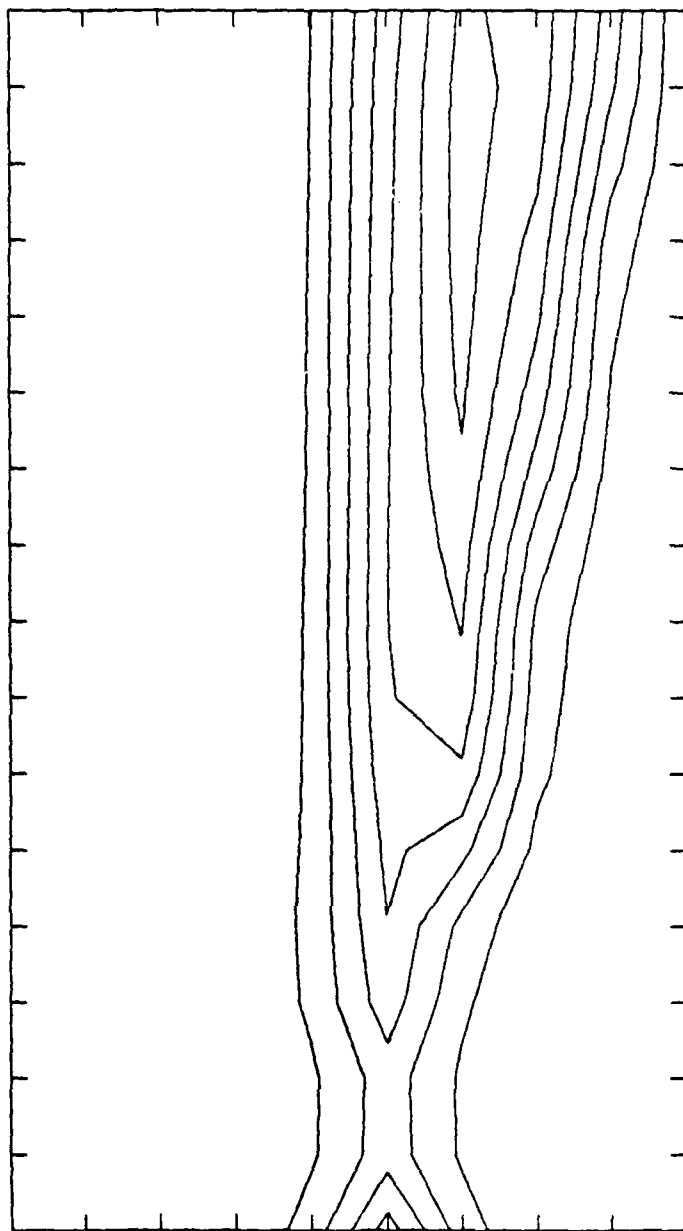


Figure 5. Orders of Magnitude of Plume Concentration with Turbulence Intensity equal to .05.

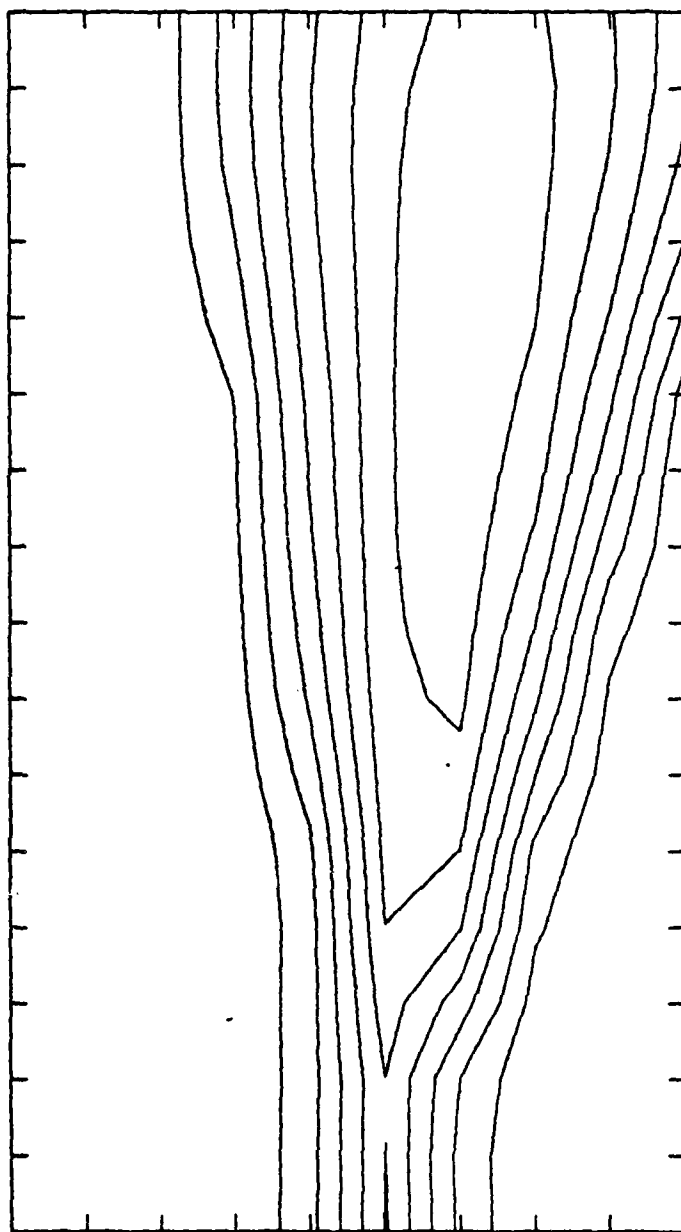


Figure 6. Same as Figure 5 except Turbulence Intensity equal to .10.

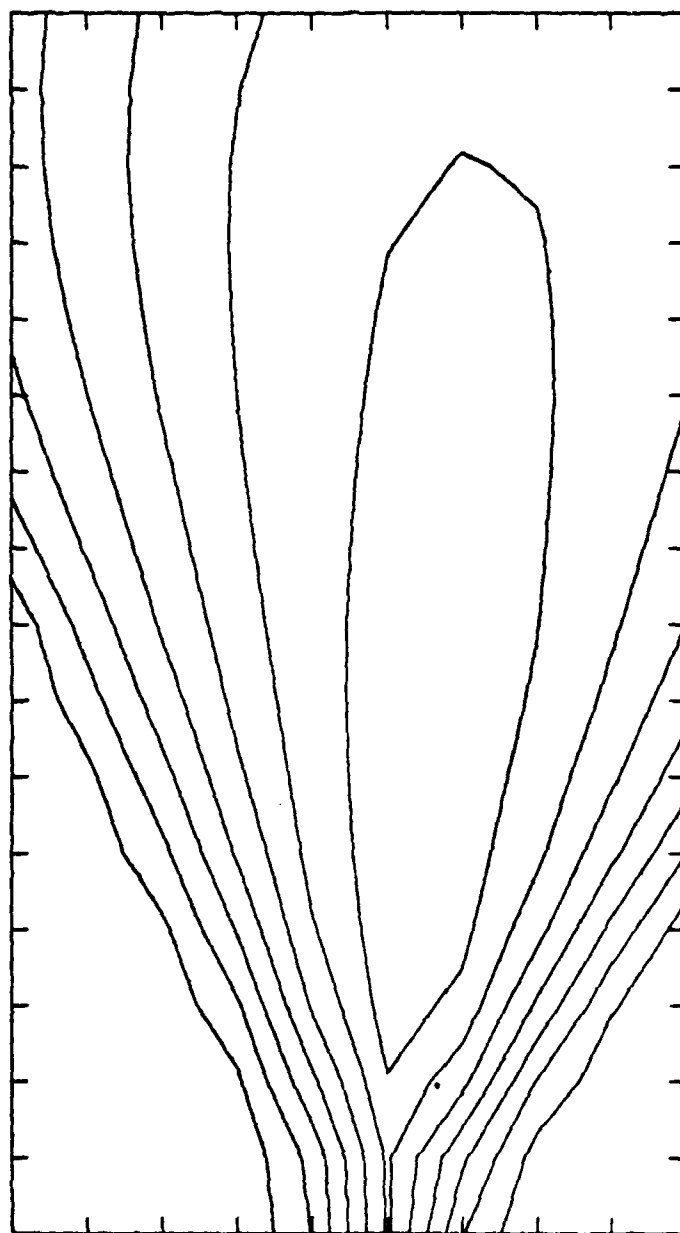


Figure 7. Same as Figure 5 except Turbulence Intensity equal to .25.

smoothing routine would tend to smooth strong concentrations near the source, the smoothing should be eliminated if the primary interest is near the source. Actually one would expect the puffs to behave as in Fig. 8, from Mikkelsen (1979), showing the relationship between the puff size and concentration, the rate of puff release ( $\tau U$ ) and the advecting wind speed  $U$ .

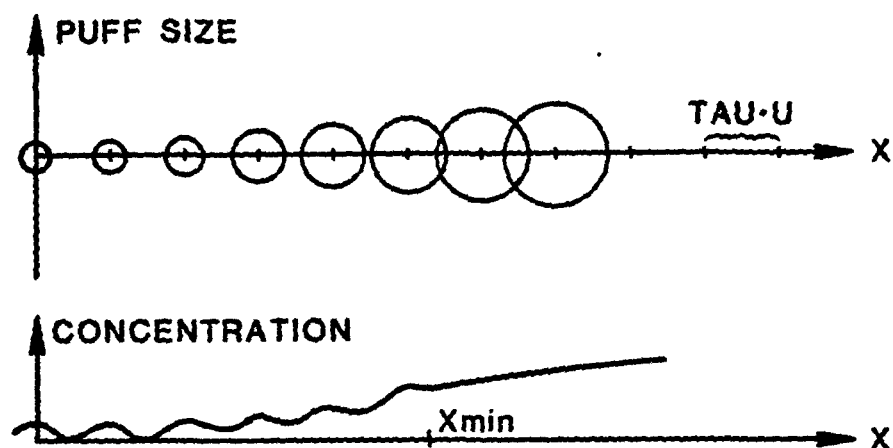


Figure 8. Relationship between Puff Size, Concentration, Puff Release Rate ( $\tau U$ ) and Advecting Wind Speed  $U$  (Mikkelsen, 1979).

Puffs would have to travel the distance  $X_{min}$  before they expand to a size where they effectively overlap and form a solid plume. From Figs. 5-7, one can see that plume concentrations have increased with distance and that a  $X_{min}$  has been reached in the middle to upper part of the grid. It is at this point that the puff model would be expected to accurately predict plume concentrations. If the area of interest is before the present  $X_{min}$ , the release rate of puffs would need to be increased so that the successive puffs would overlap sooner. Also noted that as the turbulence intensity increases, the area of maximum concentration of the plume expands while the central concentration decreases. This agrees with conservation of mass theory.

To appreciate the relative importance of the source strength and buoyant heat flux, these variables (discussed in Chapter IV) were doubled separately and together and the concentrations compared to the concentrations from the actual conditions. Little or no changes in concentration were noted when the buoyant heat flux was doubled and source strength remained the same. However, when the source strength was doubled and heat flux held constant, the grid concentrations doubled as expected. Thus, under existing

conditions, the source strength was critical to the predicted plume concentrations while the buoyant heat flux, within the range tested, was not relevant. The vertical printer plots did show an initial puff rise soon after release due to the initial heat release but as the puff rose and expanded, it soon reached the ambient temperature and leveled off. The buoyant heat flux would probably be more important when dealing with a smaller scale grid or greater heat release.

## V. DATA COMPARISON

No attempt was made to compare actual puff model concentration predictions at exact grid points to aircraft observations for the following reasons:

- The aircraft locations were approximations--the exact locations were not known. Large differences in predicted concentrations are seen with small grid separations as evidenced in Table II.
- As noted in Fig. 2, the aircraft observations were taken over a period of time at different levels--while the puff model produced multilevel instantaneous predictions.
- As mentioned earlier, the actual wind was not constant between the ship observation site and the opposite side of the grid near shore. Since the model advects the puffs based upon ship observed wind, the behavior of actual plume would be different from predicted.
- Calibration procedures for the  $\text{SF}_6$  continuous analyzer mounted onboard the aircraft were not available for instantaneous concentrations greater than 1010 PPT.

Therefore, a question of actual levels of  $\text{SF}_6$  concentration in the higher ranges exists.

The puff model predicted concentrations are expressed in  $\text{g/m}^3$  while the aircraft observations are shown as the volume of  $\text{SF}_6$  per unit volume of air in PPT. A conversion between the predicted and observed concentrations was obtained by computing the partial pressure and molecular weight of  $\text{SF}_6$  at standard pressure and temperature. A conversion of

$\text{g/m}^3 = (.63 \times 10^{-11}) \times \text{observed concentration (PPT)}$   
was thus found.

Generally, the aircraft sampled concentrations (Fig. 2) show values between 100 and 8000 PPT. Converting these observed concentrations to predicted concentration units gives values between  $.63 \times 10^{-9}$  and  $.50 \times 10^{-7} \text{ g/m}^3$ . These observed concentrations are much smaller than the values shown in Table II. Perhaps this difference could be explained by the fact that the puff model advected the plume toward the coast in the same direction under the same very stable conditions as observed on the ship. Any consideration of increased turbulence and wind shifts near shore would be expected to reduce the actual plume concentrations toward the observed concentration levels.



Increasing the turbulence intensity to 0.25 and keeping all other variables constant, the concentration values would decrease to the order of magnitude of  $10^{-6}$ --closer to the observed concentrations. (This would require the wind direction standard deviation to increase from 1 to 28). However the increased instability would cause the plume to spread over a much greater area (Fig. 7) than observed by the aircraft.

## VI. CONCLUSIONS AND RECOMMENDATIONS

The puff model has been demonstrated to be a versatile working dispersion model. Different combinations of input variables showed the expected reasonable results. The differences between model predicted and aircraft observed plume concentrations do not seem to be the fault of the model but mainly that of the highly variable meteorological conditions found along a coast.

Probably the most obvious conclusion reached from this study is that predicting the behavior of a plume moving over a marine environment onto a coastal region has significant problems. In all probability, atmospheric boundary layer conditions 7.4 km offshore can be very different from those observed in the more turbulent coastal region. The single point meteorological measurement at the source should not be expected to adequately represent plume characteristics as it nears a meteorologically variable coastline. Additional observations (primarily wind speed and direction), or other means of predicting the coastal meteorological conditions, would have to be incorporated into the puff model to adequately handle this problem.

The advantage of incorporating variable grid spacing within the puff model and the obvious benefits have already been discussed.

Presently, the mixing cap of the puff model is required to be located at an integer multiple of  $\Delta Z$ . More flexibility in this parameter to include any level, regardless of  $\Delta Z$ , would be beneficial.

Along with the puff locations shown on the lineprinter output, a maximum concentration level of each puff would be helpful.

In future experiments, several aircraft tracks should be made further out from the coast in an attempt to avoid the turbulent coastal region. Observations thus obtained in a noncoastal environment would help to verify the model predictions without the coastal influence.

## APPENDIX A

### MAJOR SECTIONS OF THE PUFF MODEL

The Risø Puff Model has been described by (Mikkelsen, 1979). The code also is well documented with comment statements. With that information and the outline to be provided in this and the following appendices, the computational and input/output procedures will be obvious.

The program and input data are stored on cards for the sake of permanency. For efficient operational execution, the program and input data cards are read on a disk within the computer. The model can then be run at will without reference to the original data cards. Minor changes can easily be made directly on the disk both to the model and/or data before each execution.

The model can be separated into the following main sections:

- A. Input Data
- B. Initial
- C. Calculating
- D. Output
- E. Error Diagnostics
- F. Subroutines

These will be described separately in the following sections.

#### A. INPUT DATA SECTION

The input data includes the variables shown in Table IV.

TABLE IV

Input Data Variables for the Puff Dispersion Model.

Wind History	Potential Temperature Gradient
Turbulence Intensity	Buoyant Heat Flux
Grid Dimensions	Minimum Concentration of Interest
Mixing Depth	Reflection at Ground Level
Source Locations, Start/Stop Time, Strength, Heat Emission	
Number of Seconds between Advection Steps	
Number of Seconds between Printouts/Plots	
Number of Seconds between Puff Releases	

The wind field and stability class for the current time step are read at the start of the calculation section.

The variables listed above are printed as a input data check and a permanent record to accompany the actual output. In most cases the print command can be overridden by YES/NO options.

#### B. INITIAL SECTION

Based upon the input data from section (A), the initial section specifies and initializes parameters to be used in

the calculating section and is passed only once during execution of the model. The grid and some counters are initialized. Constants relating to reflectance, mixing depth and stability as well as those controlling the size of some of the loops within the model are established. Parameters such as number of puff releases per second, number of advection steps per second and number of advection steps per puff release are determined.

#### C. CALCULATION SECTION

Using current wind and stability class data read at the start of the calculation section, the model advects the puff centers and calculates the growth rate and plume rise of the puffs. It removes the puffs that have left the grid (horizontally and/or vertically). The predicted concentration is computed at the grid points to include pollutants from all nearby puffs.

#### D. OUTPUT SECTION

For time intervals designated by the input data, printer plots of the X-Y and Y-Z grid are produced. A maximum mixing level is marked on the Y-Z grid if in effect.

These plots include the source location and a trace of the plume from the release time to the maptime. Also printed at this interval is a X-Y table of grid concentrations for each vertical level of interest. These concentrations can be either accumulated or actual concentrations at the plot time.

Added to the puff model is a versatic plotter routine to smooth and contour the grid magnitude concentrations of the above tables.

#### E. ERROR DIAGNOSTIC SECTION

If the model is directed by the input data beyond the limits of the design of the program, the program is terminated by way of the error diagnostic section. It prints comments relating to commonly made input errors enabling the user to isolate problems.

#### F. SUBROUTINES

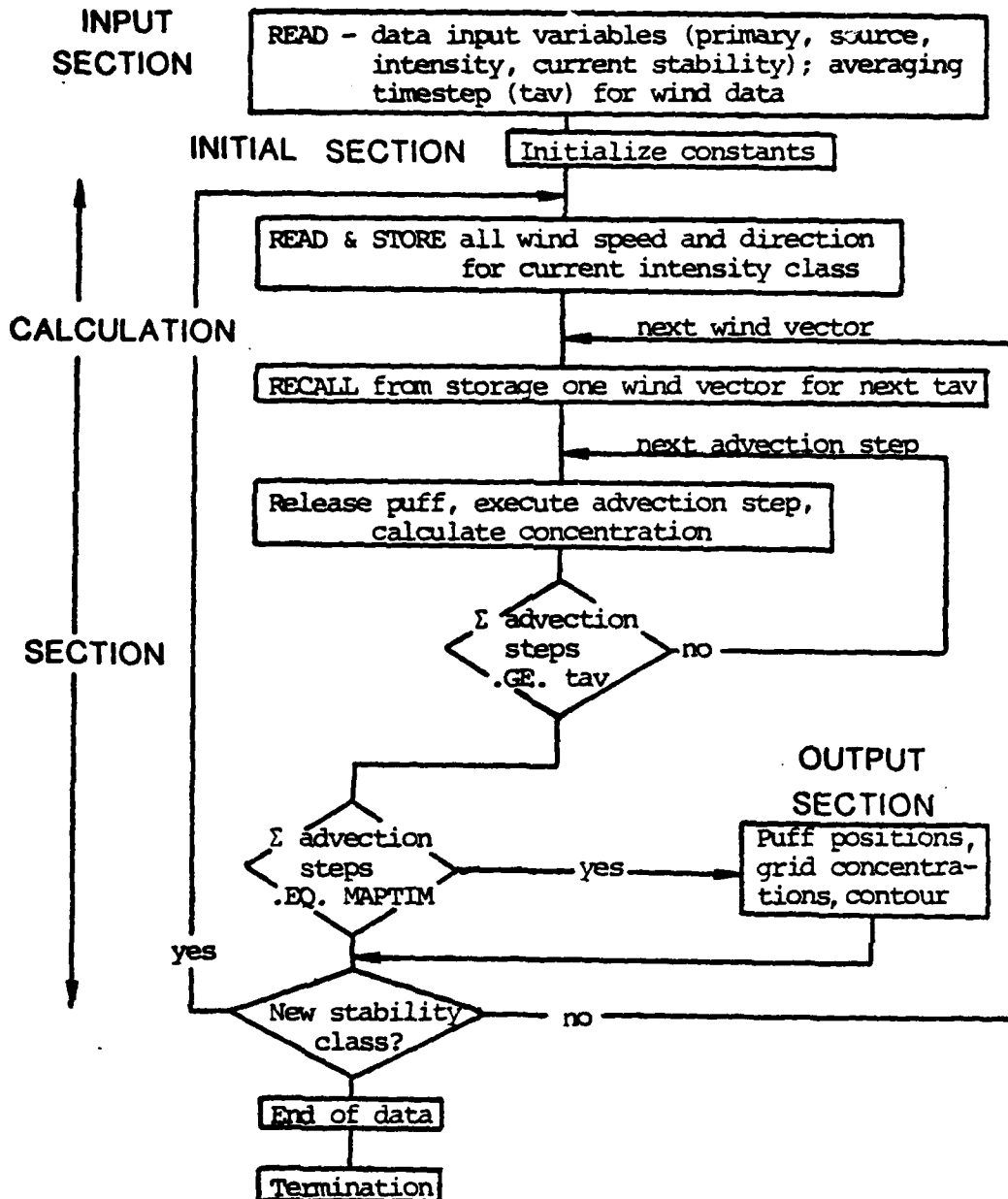
The subroutine "Sigris" calculates the puff size in the horizontal and vertical directions. It also estimates plume rise associated with pollutant buoyancy.

The subroutines "Ispace" and "Rspace" are used in the framework of the printer plots.

The subroutine "Draw" converts the plume concentrations to a logarithmic values, smoothes and then contours them using NPS inhouse contour subroutines. The values are converted to their logarithm values so that the problem of contouring over many orders of magnitude is simplified.



APPENDIX B  
PUFF MODEL FLOW CHART



APPENDIX C  
PUFF MODEL CONTRACTIONS

CHEMIN--Minimum grid concentration of interest

DELX,DELY,DELZ--Distance in meters between grid points

DOSE--Allows the concentration matrix to accumulate

DTDZ--Potential temperature gradient (K/M) (.GE. 0)

HEAT--Individual source heat emission (KW)

ICOLS--Number of columns in grid (.LE. 10)

INST--Instantaneous concentration matrix

ITIME--Start time

JROWS--Number of rows in grid

KPLANS--Number of vertical levels in grid (includes surface)

MAPTIM--Number of seconds between printer plots

NRELSE--Number of seconds to stop of release

NRMULT--Number of sources (.LE. 25)

NTADV--Integer number of seconds between advection steps

REFLEC--Reflection at ground level (0. none;1.0 total)

SOURNR--Number to identify source

SOURST--Strength for individual source (gm/s)

STOPRL--Individual source stop time (s)

STRTRL--Individual source start time (s)

TAU--Integer number of seconds between puff releases

TURN--Angle of rotation of wind direction

XSOURCE--X coordinate of source in grid units

YSOURCE--Y coordinate of source in grid units

ZN--Limited mixing depth (m)

# LISTING OF PUFF MODEL COMPUTER CODE

```

// EXEC PGM=IEBGENER
// SYSPRINT DD DUMMY
// SYSIN DD DUMMY
// SYSUT2 DD UNIT=SYSDA,DISP=(NEW,PASS),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=6400),
// SPACE=(TRK,(1,1)),DSN=&FT02
// SYSUT1 DD *
// WINDATA SEPT 29 81
// AB10929 1630 #1800#
//D
// 085*04.7" 085*04.8
//
// EXEC FRTXCLGN,NAME=CONRECQC
//FORT.SYSIN DD DUMMY
//FORD.1(KIND=DISK,TITLE='PRIMDA',FILETYPE=
//CCFILE 2(KIND=DISK,TITLE='VINDDA',FILETYPE=
//CCFILE 3(KIND=DISK,TITLE='STABDA',FILETYPE=
//CCFILE 4(KIND=DISK,TITLE='SOURCEDA',FILETYPE=
//CCFILE 5(KIND=DISK,TITLE='INTSDA',FILETYPE=
//PRINT(KIND=PRINTER,FILETYPE=7)
//CCFILE 6(KIND=PRINTER,FILETYPE=7)

```

THIS MICRODIFFUSION PROGRAM REPRESENTS THE STATE-OF-THE-ART CONCERNING THE DEVELOPMENT OF A NUMERIC DIFFUSION MODEL FOR OBSCURATION SMOKE. (RISO, MET. SEC. SEPT 1978)

THE PROGRAM IS DOCUMENTED BY HEAVY USE OF COMMENT STATEMENTS. FOR COLLECTING AN OVERALL VIEW OF THE PROGRAM STRUCTURE, AS WELL AS TO SET UP INPUT DATA FILES, IT IS ADVISED TO CONSULT THE FLOWCHARTS AND DESCRIPTIONS IN THE CONSECUTIVE REPORT.

```
COMMON HEATFX(25), I2,DMS,POINT,INTENS(14),STABPA,FBUFLX
1 SPEED,CONST1,DEL2,ANGLE,XSB,XLB,YSB,YLB,ZSB,ZLB,YINT,XINT
1 INTEGER TAU,POINT,WINDOW,TOTIM,SUMPUF,SOURNR,TPUFFS(25),XINT
1 ZMG,ZINTPF,WINDAY,YTSTRT,XSOURC(25),SIRTRL(25),STOPRL(25)
1 INTEGER XSOURC(25),SIRTRL(25),STOPRL(25)
```

```
LOGICAL LINE, COINCID, NOMXDP, GRRFLX      PUF00410
DIMENSION STRING(105), HORFRM(105), VERFRM(105), VRFRMZ(105), VRFRMZ(105) PUF00420
105), VERPLS(105), VRPLSZ(105), PARENT(105), NBUF(7), SBUF(7) PUF00430
REAL BL(105), SN1(105), SN2(105), SN3(105), SN4(105), SN5(105), SN6(105), PUF00440
```

PUF 00010  
PUF 00020  
PUF 00030  
PUF 00040  
PUF 00050  
PUF 00060  
PUF 00070  
PUF 00160  
PUF 00170  
PUF 00180  
PU00190  
PU00200  
UF 00210  
PUF 00220  
PUF 00230  
PUF 00240  
PUF 00250

PUF00280  
PUF00310  
PUF00320  
PUF00340  
PUF00350  
PUF00360  
PUF00370  
PUF00380  
UF00390

PUF00410  
PUF00420  
PUF00430  
PUF00440







```

C      OUTPRINTING CURRENT SOURCE POSITION(S) IN GRID PICTURE
C      SKIP PLOT OF SOURCE POSITIONS IF SPECIFIED IN 'RIMDA
C      IF(ABC(6) .EQ. 'NO', GO TO 999
C
C      IF(ICOLS.GT. 10) GO TO 995
860  FORMAT(1H, 49X, 33H CURRENT SOURCE DATA AS SPECIFIED, /50X, 27H IN SOURCE
865  SOURCE DATA INPUT FILE: //)
865  FORMAT(1H, 50X, 'SOURCES ARE REPRESENTED BY: ', /55X, 'STOP TIME (SEC): /55X,
1/55X, 'START TIME (SEC): /55X, 'BUOYANT HEAT FLUX: //')
2, 'SOURCE STRENGTH: /55X, 'SOURCE NUMBER: ', /55X,
C
870  FORMAT(2H, 16H Y COORDINATE OF, 25X, 32H X COORDINATE OF THE GRID
POINTS/2X, 16H THE GRID POINTS, 18, 9110/)
871  FORMAT(2H, 16H Y COORDINATE OF, 25X, 32H Z COORDINATE OF THE GRID
POINTS/2X, 16H THE GRID POINTS, 18, 9110/)
C
WRITE(6, 860)
WRITE(6, 865)
WRITE(6, 870) (I, I=XS, XLB)
WRITING DATA INTO GRIDPOINTS:
910  FORMAT(1H, 11, 5X, 2H, 105A1)
913  FORMAT(1H, 19X, 105A1)
914  FORMAT(1H, 17X, 1H, 105A1/1H, 17X, 1H, 105A1)
C
WRITE(6, 1)
WRITE(6, 912) HORFRM
WRITE(6, 913) VERFRM, VERFRM
MAX = JROWS - 1
NY5 = MAX + 1
DO 950 NY6 = 1, NY5
I = NY6 - 1
MAXMI = MAX - I
WRITE(6, 910) MAXMI, VERPLS
DO 920 J = 1, NRMULT
IF (MAX - I .NE. YSOURC(J)) GO TO 920
CALL ISPACE(XSOURC(J), J)
CONTINUE
920  WRITE(6, 913) VERFRM, VERFRM
C
DO 932 J = 1, NRMULT
IF (MAX - I .NE. YSOURC(J)) GO TO 932
WRITE(6, 914) VERFRM
CALL ISPACE(XSOURC(J), STRIRL(J))
CONTINUE
932  WRITE(6, 913) VERFRM, VERFRM

```

PUF01920  
 PUF01930  
 PUF01940  
 PUF01950  
 PUF01970  
 PUF01980  
 PUF01990  
 PUF02000  
 PUF02010  
 PUF02050  
 PUF02060  
 PUF02070  
 PUF02080  
 PUF02090  
 PUF02100  
 PUF02110  
 PUF02120  
 PUF02130  
 PUF02140  
 PUF02150  
 PUF02160  
 PUF02170  
 PUF02190  
 PUF02200  
 PUF02210  
 PUF02220  
 PUF02230  
 PUF02240  
 PUF02250  
 PUF02260  
 PUF02270  
 PUF02280  
 PUF02290  
 PUF02300  
 PUF02310  
 PUF02320  
 PUF02330  
 PUF02340  
 PUF02350  
 PUF02360  
 PUF02370  
 PUF02380  
 PUF02390  
 PUF02400  
 PUF02410



```

C      DO 934 J = 1,NRMULT
      IF(MAX-I.NE.YSOURC(J)) GO TO 934
      WRITE(6,914) VERFRM
      CALL ISPACE(XSOURC(J),STOPRL(J))
      CONTINUE
934    WRITE(6,913) VERFRM,VERFRM
C
      DO 940 J=1,NRMULT
      IF(MAX-I.NE.YSOURC(J)) GO TO 940
      WRITE(6,914) VERFRM
      CALL RSPACE(XSOURC(J),SOURST(J))
      CONTINUE
940    WRITE(6,913) VERFRM,VERFRM
C
      DO 930 J=1,NRMULT
      IF(MAX-I.NE.YSOURC(J)) GO TO 930
      WRITE(6,914) VERFRM
      CALL RSPACE(XSOURC(J),HEATFX(J))
      CONTINUE
930    WRITE(6,913) VERFRM,VERFRM
C
      CONTINUE
      WRITE(6,1)
      WRITE(6,912) HORFRM
C
      GO TO 999
990    FORMAT(53H SOURCE DATA PLOT SUPPRESSED BECAUSE"ICOLS"EXCEEDS 10)
995    WRITE(6,990)
999    CONTINUE
C
      DEFINE STABILITY AND INTENSITY CLASSES
      INPUT FROM INTENSITY - DATA: INTSDA
C
960    FORMAT(14,F5.4)
965    FORMAT(1H0, 46H IN THE CURRENT RUN, THE STABILITY-CLASSES ARE,/41H
      CONNECTED TO INTENSITY DATA AS FOLLOWS:)
970    FORMAT(1H, 21H STABILITY CLASS NO. :,13,1315)
975    FORMAT(1H, 21H INTENSITY DATA :, 14F5.4)
C
      READ INTSDA TITLE-STRING:
      READ(5,30) INSTX
      WRITE(6,30) INSTX
      READ INTSDA, NO OF INTENSITY-CLASSES: NRINCL
      READ(5,800) ABC(3),NRINCL,ABC(4)
      WRITE(6,802) NRINCL
      INPUT FORMATE TESTING:

```

```

PUF02420
PUF02430
PUF02440
PUF02450
PUF02460
PUF02470
PUF02480
PUF02490
PUF02500
PUF02510
PUF02520
PUF02530
PUF02540
PUF02550
PUF02560
PUF02570
PUF02580
PUF02590
PUF02600
PUF02610
PUF02620
PUF02630
PUF02640
PUF02660
PUF02670
PUF02680
PUF02700
PUF02710
PUF02720
PUF02730
PUF02740
PUF02750
PUF02760
PUF02770
PUF02780
PUF02790
PUF02800
PUF02810
PUF02820
PUF02830
PUF02840
PUF02850

PUF02870
PUF02880

PUF02890

```







```

BACKSPACE 2
IF (TYPE(1).EQ.ANFO) READ(2,1131)(NBUF(1),SBUF(1),I=1,7)
IF (TYPE(1).EQ.ANFO) WRITE(6,1131)(NBUF(1),SBUF(1),I=1,7)
IF (TYPE(1).EQ.SLASH) READ(2,1130)
1131 FORMAT(7I4,1X,F4,1)
C LOOP THRU WINDDATA AT SPECIFIED TIMESTEPS
I = 1
IF (TYPE(1).NE.SLASH) GO TO 1150
NRSTAB = NRSTAB + 1
C
C COUNTING NUMBER OF WINDDATA SPECIFICATIONS: IWDASP
IWDASP = 0
C READING STABILITY CATEGORY FROM WINDDATA:
CLASS = DATA(1)
IF (CLASS.EQ. A ) POINT = 1
IF (CLASS.EQ. B ) POINT = 2
IF (CLASS.EQ. C ) POINT = 3
IF (CLASS.EQ. D ) POINT = 4
IF (CLASS.EQ. E ) POINT = 5
IF (CLASS.EQ. PUNK) GO TO 8930
IF (CLASS.EQ. BLANK) GO TO 8940
1140 FORMAT(53H PROGRAM STOPPED ORDINARILY FM WINDDATA SPECIFICATION)
WRITE(6,1)
WRITE(6,1141) NRSTAB, POINT
WRITE(6,1)
1141 FORMAT(4H THE,13,38H. STABILITY SPECIFICATION :LASS IS NO.,11)
GO TO 1135
C INPUT STRUCTURE TEST:
1150 IF (TYPE(1).NE.ANFO .OR. TYPE(1+1).NE.ASTER) GO TO 1160
C
C IWDASP = IWDASP + 1
C CURRENT WINDDATA:
JI = (I+1)/2
ANGLE = NBUF(JI)
SPEED = SBUF(JI)
GO TO 1175
1160 IF (TYPE(1).NE.BLANK .OR. TYPE(1+1).NE.BLANK) GO TO 8950
C READ NEW DATA IN LINE 1135
GO TO 1135
C INDATA PART OF PROGRAM TERMINATED.
1175 CONTINUE
C
C CURRENT WINDDATA PRESENT.
C
C OUTPRINTING CURRENT WINDDATA:
WRITE(6,1161) IWDASP ,ANGLE, SPEED
C

```

PUF04350  
 PUF04360  
 PUF04370  
 PUF04380  
 PUF04390  
 PUF04400  
 PUF04410  
 PUF04420  
 PUF04430  
 PUF04440  
 PUF04450  
 PUF04460  
 PUF04470  
 PUF04480  
 PUF04490  
 PUF04500  
  
 PUF04530  
 PUF04540  
 PUF04550  
 PUF04560  
 PUF04570  
 PUF04580  
 PUF04590  
 PUF04600  
 PUF04610  
 PUF04620  
 PUF04630  
 PUF04640  
 PUF04650  
 PUF04660  
 PUF04670  
 PUF04680  
 PUF04690  
 PUF04700  
 PUF04710  
 PUF04720  
 PUF04730  
 PUF04740  
 PUF04750  
 PUF04760  
 PUF04770  
 PUF04780

```

C C CALCULATING WIND VELOCITY IN GRID UNITS: VGX,VGY
C C VGX = SPEED*(COS(ANGLE*3.142/180)) / DELX
C C VGY = SPEED*(SIN(ANGLE*3.142/180)) / DELY
C C RENAMING WIND AVERAGING TIME:WINDAV AS TAV:
C C TAV = WINDAV
C C 1161 FORMAT(4H THE, I4, 49H WINDDATASET IN THE CURRENT STAB.CLASS IS: ANG
C C 1161 LE=, I4, 8H , SPEED=, F4.1)
C C LOOP THRU BASIC ADVECTION STEPS WITH CURRENT WIND FIELD
C C DO 5000 NN=1,NADPRW
C C JUMPING OVER "ZERO-SETTING" OF CONCENTRATION MATRIX : CHI , IF
C C "DOSE MODE" IS SPECIFIED IN PRIMDA.
C C IF(ABC(8).EQ. DOSE ) GO TO 1256
C C DO 1255 IG=1,ICOLS
C C DO 1255 JG=1,JROWS
C C DO 1255 KG=1,KPLANS
C C 1255 CHI(IG,JG,KG) = 0.0
C C 1256 CONTINUE
C C TIMECOUNTER:TOTTIM (SEC.)
C C TOTTIM = TOTTIM + NIADV
C C SKIPPING RELEASE-SECTION IF SPECIFIED
C C IF(TOTTIM.GT. NRELS) GO TO 1250
C C TESTING IF RELEASE CONDITIONS ARE FULFILLED
C C IF(MOD(TOTTIM,TAU) .NE. 0) GO TO 1250
C C LOOP THRU MULTIPLE SOURCES
C C DO 1250 I2 = 1,NRMULT
C C INDIVIDUAL RELEASE CONTROL AS SPECIFIED IN SOURCE DATA:
C C IF((TOTTIM.LT.STRTRL(I2)).OR. (TOTTIM.GT.STRPRL(I2))) GO TO 1250
C C TOTAL NUMBER RELEASED FROM SOURCE(I2): TPUFFS(I2):
C C TPUFFS(I2) = TPUFFS(I2) + 1
C C SHIFTING PUFF TABLE ONE POSITION TO THE RIGHT AND THEREBY
C C GIVING SPACE FOR ONE NEW PUFF:
C C J=1
C C 1204 DO 1205 K=1,7
C C 1205 SHIF(T(J+1,K) = PTABEL(I2,J,K)
C C J = J + 1

```

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PUF04790
PUF04800
PUF04810
PUF04820
PUF04830
PUF04840
PUF04850
PUF04860
PUF04870
PUF04880
PUF04900
PUF04920
PUF04940
PUF04950
PUF04960
PUF04970
PUF04980
PUF04990
PUF05000
PUF05010
PUF05020
PUF05030
PUF05040
PUF05050
PUF05060
PUF05080
PUF05090
PUF05100
PUF05110
PUF05130
PUF05140
PUF05150
PUF05170
PUF05180
PUF05190
PUF05200
PUF05210
PUF05220
PUF05230
PUF05240
PUF05250
PUF05260
PUF05270
PUF05280
PUF05290

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```

IF(J,GE,100) GO TO 8900
IF(PTABEL(I2,J,1)) .NE. 0) GO TO 1204
DO 1210 L = 2,J
1209 DO 1210 K = 1,I
1210 PTABEL(I2,L,K) = SHIFT(L,K)
C
C      INSERTING NEW PUFF DATA IN PUFF TABLE AT J = I
PTABEL(I2,1,1) = TPUFFS(I2)
C      DOSE RELEASED WITH EACH PUFF: SPECIFIED SOURCE STRENGTH*SEC.
C      BETWEEN RELEASES
PTABEL(I2,1,2) = SOURST(I2) * TAU
C
C      LOADING IN INITIAL SOURCE POSITIONS
PTABEL(I2,1,3) = XSOURC(I2)
PTABEL(I2,1,4) = YSOURC(I2)
C
C      TO AVOID NUMERICAL PROBLEMS IN ESTIMATING PLUME RISE,
C      SET S0HT(I2) (SOURCE HEIGHT) .GE. 1 METER.
PTABEL(I2,1,5) = S0HT(I2)/DELZ
C      INITIAL SIZE OF PUFFS:
C      SIGMAXY SET TO 1 METER:
PTABEL(I2,1,6) = 1
C      SIGMAZ SET TO 1 METER:
PTABEL(I2,1,7) = 1
C      END OF PUFF RELEASE SECTION.
C 1250 CONTINUE
C
C      ADVECTION OF ALL PUFF CENTERS
C
C      ADVANCE OF PUFF CENTERS IN GRID UNITS (HORIZONTALLY)
DGX = VGX*NTADV
DGY = VGY*NTADV
C      TOTALY TRAVELED DISTANCE BY THE PUFFS IN METERS
C      DURING CURRENT BASIC ADVECTION STEP: DMS
DMS = SQR((DGX*DELX)**2 + (DGY*DELY)**2)
C
C      ADVECTION SECTION FOR ALL EXISTING PUFFS:
C      LOOP THRU ALL SOURCES, COUNTING REMOVED PUFFS:LEAVE
DO 1300 I2 = 1, NRMULT
J = 1
C      SKIPPING SOURCE I2, IF THE LAST BORN PUFF HAS LEFT GRID
IF(PTABEL(I2,1,1).EQ.0) GO TO 1300
PTBL3 = PTABEL(I2,J,3) + DGX
PTBL4 = PTABEL(I2,J,4) + DGY
1260
C
C      CALLING SUBROUTINE "SIGRIS" THEREBY ADDING DEVIATION INCREMENT
C      AND PLUME RISE INCREMENT TO PUFF TABLE:

```

PUF 05300  
 PUF 05310  
 PUF 05320  
 PUF 05330  
 PUF 05340  
 PUF 05350  
 PUF 05380  
 PUF 05390  
 PUF 05410  
 PUF 05420  
 PUF 05430  
 PUF 05440  
 PUF 05450  
 PUF 05460

PUF 05500  
 PUF 05510  
 PUF 05520  
 PUF 05530  
 PUF 05540  
 PUF 05550  
 PUF 05560  
 PUF 05570  
 PUF 05580

PUF 05630  
 PUF 05650  
 PUF 05660

PUF 05680  
 PUF 05690  
 PUF 05700  
 PUF 05720  
 PUF 05730  
 PUF 05740  
 PUF 05750

PUF 05770  
 PUF 05780  
 PUF 05790  
 PUF 05800  
 PUF 05840  
 PUF 05850  
 PUF 05860

```

C      PTABEL(I2,J,5): Z-POSITION IN GRIDUNITS
C      PTABEL(I2,J,6): SIGMAX IN METERS
C      PTABEL(I2,J,7): SIGMAZ IN METERS
C
C      CALL SIGRIS(PTABEL(I2,J,5),PTABEL(I2,J,6),PTABEL(I2,J,7))
C
C      INTRODUCING AN UPPER LIMIT FOR BUOYANCY CONVECTION: ZM
C      IF(.NOT.NOMXDP.AND.PTABEL(I2,J,5).GT.ZMG) PTABEL(I2,J,5) = ZMG
C
C      Z - POSITIONS IN GRIDUNITS: PTBL5
C      PTBL5 = PTABEL(I2,J,5)
C
C      TESTING AND REMOVING PUFFS WHICH HAVE LEFT THE GRID:
C      IF(PTBL3.GT.XSB.AND.PTBL3.LT.XLB.AND.PTBL4.GT.YBB.AND.PTBL4.LE.YL
C      1L.AND.PTBL5.LT.ZLB) GO TO 1290
C
C      REMOVE SECTION
C      LEAVE = LEAVE + 1
C      IF(PTABEL(I2,J+1,1).EQ.0) GO TO 1265
C      REMOVING PUFF BORN AT SOURCE I2 WHICH IS NOT THE LONGEST LIVING:
C      LEFT JUSTIFICATION OF OLDER PUFFS:
C      JJ = J + 1
C      1269 DO 1270 K = 1,7
C      1270 SHIFT(JJ,K) = PTABEL(I2,JJ,K)
C      JJ = JJ + 1
C      IF(PTABEL(I2,JJ,1).NE.0) GO TO 1269
C      SHIFT(JJ,1) = 0
C      JMAX = JJ
C      COPY SHIFT BACK INTO PTABEL:
C      NY7 = JMAX - 1
C      DO 1275 JJ = J, NY7
C      DO 1275 K = 1,7
C      1275 PTABEL(I2,JJ,K) = SHIFT(JJ+1,K)
C
C      RETURNING TO INCREMENTAL PART WITHOUT INCREASE IN J:
C      GO TO 1260
C
C      REMOVING LONGEST LIVING PUFF FROM SOURCE(I2):
C      1265 PTABEL(I2,J,1) = 0
C      CONTINUING WITH NEXT SOURCE
C      GO TO 1300
C
C      REPLACING NEW PUFF POSITION IN PUFF TABLE
C      1290 PTABEL(I2,J,3) = PTBL3
C      PTABEL(I2,J,4) = PTBL4
C
C      CALCULATING GRID CONCENTRATION IN EACH BASIC ADVECTION STEP

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PUF05870  
 PUF05880  
 PUF05890  
 PUF05900  
 PUF05910  
 PUF05920  
 PUF05930  
 PUF05940  
 PUF05950  
 PUF05960  
 PUF05970  
 PUF05980  
 PUF05990  
 PUF06000  
 PUF06010  
 PUF06020  
 PUF06030  
 PUF06040  
 PUF06050  
 PUF06060  
 PUF06070  
 PUF06080  
 PUF06090  
 PUF06100  
 PUF06110  
 PUF06120  
 PUF06130  
 PUF06140  
 PUF06150  
 PUF06160  
 PUF06170  
 PUF06180

PUF06200  
 PUF06210  
 PUF06220  
 PUF06230  
 PUF06240  
 PUF06250  
 PUF06260  
 PUF06270  
 PUF06280  
 PUF06290  
 PUF06300  
 PUF06310  
 PUF06320  
 PUF06330  
 PUF06340  
 PUF06350  
 PUF06360  
 PUF06370  
 PUF06380  
 PUF06390  
 PUF06400



```

C C RENAMING ESSENTIAL PARAMETERS:
C C DOSE IN CURRENT PUFF:
C C Q1 = PTABEL(I2,J,2)
C C SIGMA VALUES IN METERS:
C C SIGMXY = PTABEL(I2,J,6)
C C SIGMZ = PTABEL(I2,J,7)
C C CALCULATING MAXIMUM CONCENTRATION IN EACH PUFF CENTER
C C (PUFF-CHI-CENTER) ; IN DIMENSION: GRAM/M**3 :
C C CONSTANT : (2*PHI)**(3/2)
C C CONST = 15.7496
C C PCHCEN = Q1/(CONST*SIGMZ*SIGMXY**2)
C C SKIPPING SUMMATION SECTION IF CONCENTRATION IS TOO LOW
C C IF(PCHCEN.LT.CHEMIN) GO TO 1500
C C CALCULATING MAXIMUM RADIUS OF INTEREST FOR EACH PUFF:
C C MAXIMUM PUFF RADIUS IN METERS:
C C PFRMXY = SIGMXY * SQRT(-2.*ALOG(CHEMIN/PCHCEN))
C C PFRMZ = PFRMXY*SIGMZ/SIGMXY
C C X-DIRECTION:
C C PUFRGX = PFRMXY/DELX
C C Y-DIRECTION:
C C PUFRGY = PFRMXY/DELY
C C Z-DIRECTION:
C C PUFRGZ = PFRMZ/DELZ
C C DETERMINING START AND STOP GRID POINTS FOR ACCUMULATION OF
C C THE PUFFS IN QUESTION:
C C ISTRTX = PTBL3 - PUFRGX + 1
C C ISTOPX = PTBL3 + PUFRGX + 1
C C ISTRTY = PTBL4 - PUFRGY + 1
C C ISTOPY = PTBL4 + PUFRGY + 1
C C ISTRTZ = PTBL5 - PUFRGZ + 1
C C ISTOPZ = PTBL5 + PUFRGZ + 1
C C CONTROL FOR EXCEEDING GRID DIMENSIONS
C C IF(ISTRTX.LT.XSB) ISTRTX=XSB
C C IF(ISTOPX.GT.XLB) ISTOPX=XLB
C C IF(ISTRTY.LT.YSB) ISTRTY=YSB
C C IF(ISTOPY.GT.YLB) ISTOPY=YLB
C C IF(ISTRTZ.LT.ZSB) ISTRTZ=ZSB
C C IF(ISTOPZ.GT.ZLB) ISTOPZ=ZLB
C

```

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PUF06430
PUF06440
PUF06450
PUF06460
PUF06470
PUF06480
PUF06490
PUF06510
PUF06520
PUF06530
PUF06540
PUF06550
PUF06560
PUF06570
PUF06590
PUF06600
PUF06610
PUF06620
PUF06630
PUF06640
PUF06650
PUF06660
PUF06670
PUF06680
PUF06690
PUF06700
PUF06710
PUF06720
PUF06730
PUF06740
PUF06750
PUF06760
PUF06770
PUF06780
PUF06790
PUF06800
PUF06810
PUF06820
PUF06830
PUF06840
PUF06850
PUF06860
PUF06870
PUF06880
PUF06890
PUF06900
PUF06910

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C      UPPER LIMIT IN CASE OF SPECIFIED MIXING DEPTH:ZM
C      IF(ISTRTZ.GT.ISTOPZ) AND, ISTOPZ:GT.ZMG ) ISTOPZ = ZMG
C      IF(ISTRTZ.GT.ISTOPZ) GO TO 1500
C      CALCULATE CONTRIBUTIONS TO SURROUNDING GRIDPOINTS
C      PRELIMINAR CALCULATIONS:
C      SIGMAS IN GRIDPOINTS:
C      SIGGX = SIGMX/DELX
C      SIGGY = SIGMY/DELY
C      SIGGZ = SIGMZ /DELZ
C      CALCULATING DENOMINATOR UNDER EXP-SIGN:
C      SIGGX2 = (SIGGX**2)*(-2)
C      SIGGY2 = (SIGGY**2)*(-2)
C      SIGGZ2 = (SIGGZ**2)*(-2)
C      LOOPING THRU ALL GRIDPOINTS OF INTEREST:
C      DO 1500 KG = ISTRTZ,ISTOPZ
C      ZG2NEG = (KG-PTBL5)**2
C      PCHI1 = PCHCEN * EXP(ZG2NEG/SIGGZ2)
C      IF(GRRFLX) PCHI1 = PCHI1 + PCHCEN*REFLEC*EXP((KG+PTBL5)**2/SIGGZ2)
C      IF(NOMXDP) GO TO 1295
C      IF((PTBL5+PUFRGZ).LT.ZMG) GO TO 1295
C      ZG2MX = (KG+PTBL5-2*ZMG)**2
C      PCHI1 = PCHI1 + PCHCEN*EXP(ZG2MX/SIGGZ2)
C      DO 1500 IG = ISTRTX,ISTOPX
C      XG2 = (IG-PTBL3)**2
C      DO 1500 JG = ISTRTY,ISTOPY
C      YG2 = (JG-PTBL4)**2
C      INDIVIDUAL PUFFS CONTRIBUTION : PCHI,GRAM/M**3
C      PCHI = PCHI1 * EXP(XG2/SIGGX2 + YG2/SIGGY2)
C      IF(PCHI.LT.CHEMIN) GO TO 1500
C      ACCUMULATING IN GRIDPOINTS:
C      CHI(IG+1,JG+1,KG+1) = CHI(IG+1,JG+1,KG+1) + PCHI
C      1500 CONTINUE
C      END OF CONCENTRATION CALCULATIONS
C      ADVANCE IN PUFF TABLE (J) DURING BASIC ADVECTION STEP
C      J = J + 1

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PUF06940  
 PUF06950  
 PUF06960  
 PUF06970  
 PUF06980  
 PUF06990  
 PUF07000  
 PUF07010  
 PUF07020  
 PUF07030  
 PUF07040  
 PUF07050  
 PUF07060  
 PUF07070  
 PUF07080  
 PUF07090  
 PUF07100  
 PUF07110  
 PUF07120  
 PUF07130  
 PUF07140  
 PUF07150  
 PUF07160  
 PUF07170  
 PUF07180  
 PUF07190  
 PUF07200  
 PUF07210  
 PUF07220  
 PUF07230  
 PUF07240  
 PUF07250  
 PUF07260  
 PUF07270  
 PUF07280  
 PUF07290  
 PUF07300  
 PUF07310  
 PUF07320  
 PUF07330  
 PUF07340  
 PUF07350  
 PUF07360  
 PUF07370  
 PUF07380  
 PUF07410  
 PUF07440  
 PUF07450  
 PUF07460



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C      MAX = JROWS - 1
C      OUTER LOOP THRU INTEGER Y-VALUES:
C      NY8=MAX+1  NY9=1,NY8
C      DO 1350
C      I2=NY9-1
C      MAXI2 = MAX - I2
C      WRITE(6,1327) MAXI2 , VERPLS
C
C      PLOTTING SOURCE POSITIONS
C      K1 = 0
C      DO 1330 J = 1,NRMULT
C      IF (MAX-I2,NE,YSOURC(J) ) GO TO 1330
C      NUMBER OF SOURCES IN MAINLINE: K1
C      K1 = K1 + 1
C      CALL ISPACE(XSOURC(J),J)
C      SOURCE POSITIONS IN EACH MAINLINE: XINT(K1)
C      XINT(K1) = 10*XSOURC(J)
C      CONTINUE
C      1330
C
C      LOOPING 9 LINES DOWN TO NEXT MAINLINE:
C      DO 1345 NY10=1,10
C      IDECI=NY10-1
C      YLINE = 10*(MAX - I2) - IDECI + 10
C      IF (IDECI .GE. 1) WRITE(6,1326) VERFRM
C
C      SCANNING THRU WHOLE PUFF TABLE
C      DO 1340 II = 1,NRMULT
C      J = 0
C      J = J + 1
C      IF (PTABEL(II,J,1) .EQ. 0) GO TO 1340
C      TRUNCATING Y-VALUE OF PUFF TO INTEGER:
C      YINT = PTABEL(II,J,4)*10 + 10.5
C
C      PRINTING "*" IN GRIDFRAME IF X-POSITION OF PUF= NOT COINCIDE
C      WITH ONE OF THE SOURCE POSITIONS
C      IF ( (YINT .NE. YLINE) .OR. (IDECI .NE. 0) ) GO TO 1338
C      COINCED = .FALSE.
C      INTEGER = VALUE OF PUFFS X-POSITION: XINTPF
C      XINTPF = PTABEL(II,J,3) * 10 + .5
C      DO 1336 KK = 1,K1
C      1336 IF (XINTPF .EQ. XINT(KK)) COINCED = .TRUE.
C      IF (COINCED) GO TO 1335
C      STRING(XINTPF + 1) = SNI
C      GO TO 1335
C
C      1338 IF (YINT .NE. YLINE) GO TO 1335
C      PRINTING PUFF POSITIONS BETWEEN Y-GRID LINES:
C      XINTPF = PTABEL(II,J,3) * 10 + .5

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PUF07960

PUF08000  
PUF08010  
PUF08020  
PUF08030  
PUF08040  
PUF08050  
PUF08060  
PUF08070  
PUF08080  
PUF08090  
PUF08110  
PUF08120  
PUF08130  
PUF08140

PUF08160  
PUF08170  
PUF08180  
PUF08190  
PUF08200  
PUF08210  
PUF08220  
PUF08230  
PUF08240  
PUF08250  
PUF08260  
PUF08270  
PUF08280  
PUF08290  
PUF08300  
PUF08310  
PUF08320  
PUF08330  
PUF08340  
PUF08350  
PUF08360  
PUF08370  
PUF08380  
PUF08400

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      STRING(XINTPF + 1) = SN1
      GO TO 1335
C 1340 CONTINUE
C 1341 END OF PUFF TABLE LOOP.
C
      WRITE(6,1325) STRING
      DO 1342 NST = 1,105
      1342 STRING(NST) = BL
C 1345 CONTINUE
C
      RESET "SOURCE IN LINE COUNTER" XINT(KK)
      DO 1349 KK=1,10
      1349 XINT(KK) = -1
C 1350 CONTINUE
C 1351 END OF PUFF POSITION PLOT.
      WRITE(6,1)
      WRITE(6,912) HORFRM
      1400 CONTINUE
C
      PLOTTING PUFFS IN "Y-Z FRAME"; FOR COMMENTS REFER TO THE EQUI-
      VALENT "Y-X FRAME" PLOTTING DESCRIBED ABOVE.
C
      WRITE(6,1)
      WRITE(6,1)
      WRITE(6,1)
      881 FORMAT(1H+120X,15,10H SOURCE(S))
      WRITE(6,1)
      HORFRM2: STRING CONTAINING HORIZONTAL GRID FRAME
      DO 1410 N = 1,105
      VRFRM2(N) = BL
      VRPLS2(N) = BL
      PARENT(N) = BL
      HRFRM2(N) = BL
      NY11=HFZ+10
      DO 1418 IHFZ = MSZ,NY11,10
      NY12=IHFZ+4
      DO 1411 MN = IHFZ,NY12
      HRFRM2(MN) = SN4
      1411 HRFRM2(IHFZ+5) = SN2
      NY13=IHFZ+6
      NY14=IHFZ+9
      DO 1416 MM=NY13,NY14
      HRFRM2(MM) = SN4
      1416

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PUF084430
PUF084440
PUF084450
PUF084460
PUF084470
PUF084480
PUF084490
PUF084500
PUF084510
PUF084520
PUF084530
PUF084540
PUF084550
PUF084560
PUF084570
PUF084580
PUF084590
PUF084600
PUF084610
PUF084620
PUF084630
PUF084640
PUF084650
PUF084660
PUF084670
PUF084680
PUF084690
PUF084700
PUF084710
PUF084720
PUF084730
PUF084740
PUF084750
PUF084760
PUF084770
PUF084780
PUF084790
PUF084800
PUF084810
PUF084820
PUF084830
PUF084840
PUF084850
PUF084860
PUF084870
PUF084880
PUF084890

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1418 CONTINUE 912) HRFRMZ
WRITE(6,10)ZMG + 1) = SN6
PARENT(10)MFZ + 3) = SN5
VRFRMZ(10)MFZ + 3) = SN3
VRPLSZ(10)MFZ + 3) = SN3
WRITE(6,1326) VRFRMZ
MAX = JROWS-1
DO 1445 NY15=1,JROWS
  I2=NY15-1
  MAXI2 = MAX - I2
  WRITE(6,1327) MAXI2,VRPLSZ
  K1=0
DO 1430 J=1,NRMULT
  IF (MAX-I2 .NE. YSOURC(J)) GO TO 1430
  K1 = K1 + 1
C CONTINUE NUMBER OF SOURCES IN EACH Y-GRIDLINE: VN SOURCE(S)
  IF (K1 .GT. 0) WRITE(6,881) K1
  DO 1445 NY16=1,10
    IDECI=NY16-1
    YLINE = 10*(MAX-I2) - IDECI + 10
    IF (IDECI .GE. 1) WRITE(6,1326) VRFRMZ
    ILLUSTRATING MIXING DEPTH IN Y-Z FRAME:
    IF (ZMG .GT. 0) WRITE(6,1328) PARENT
    DO 1440 JJ = 1,NRMULT
      J=0
1435 J = J + 1
      IF (PTABEL(11,J)) .EQ. 0) GO TO 1440
      YINT = PTABEL(11,J) * 10 + 10.5
      IF (YINT .NE. YLINE) GO TO 1435
      ZINTPF = PTABEL(11,J,5) * 10 + .5
      STRING(ZINTPF + 1) = SN1
      GO TO 1435
C CONTINUE
1440 CONTINUE
C WRITE(6,1325) STRING
DO 1442 NS1 = 1,105
  STRING(NS1) = BL
C CONTINUE
1445 CONTINUE
C WRITE(6,1)
  WRITE(6,912) HRFRMZ
C SECTION FOR OUTPRINTING GRID CONCENTRATIONS

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```

PUF08900
PUF08910
PUF08920
PUF08930
PUF08940
PUF08950
PUF08960
PUF08970

PUF08980
PUF08990
PUF09000
PUF09010
PUF09020
PUF09030
PUF09040
PUF09050
PUF09060

PUF09080
PUF09090

PUF09110
PUF09120
PUF09130
PUF09140
PUF09150
PUF09160
PUF09170
PUF09180
PUF09190
PUF09200
PUF09210
PUF09220
PUF09230
PUF09240
PUF09250
PUF09260
PUF09270
PUF09280
PUF09290
PUF09300
PUF09310
PUF09320
PUF09330
PUF09350

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C      SKIPPING CONCENTRATION PRINTING IF SPECIFIED IN PRIMDA.
C      IF(ABC(9).EQ.NO) GO TO 1600
C
C 1510 FORMAT(1H0,49X,37H PRINT OF CURRENT GRID CONCENTRATIONS,/50X
C 16,29H SEC. AFTER START OF RELEASE.)
C 1520 FORMAT(1H0,49X,32H GRID CONCENTRATION IN THE PLANE: ,51X,3HZ =F6.2
C 125H METER ABOVE THE SURFACE.)
C 1525 FORMAT(11,8X,10E10.2)
C
C      WRITE(6,1301)
C      WRITE(6,1510) ITOTIM
C      WRITE(6,1)
C      WRITE(6,1)
C
C      LOOP THRU ALL Z LEVELS
C
C      DO 1550 KC=1,KPLANS
C      DEMKMI = DELZ*(KC-1)
C      WRITE(6,1520) DEMKMI
C      WRITE(6,1)
C      WRITE(6,870) (IC,IC = XSB,XLB)
C      PRINTING EACH LINE IN CONCENTRATION TABLE:
C      DO 1560 JC = 1,JROWS
C      JJC = JRCWS - JC
C      JJC = JJC + 1
C      WRITE(6,1525) JJC, (CHI(IC,JCI,KC), IC = MSX,MFX)
C      DO 1551 IC=MSX,MFX
C      CPLLOT(IC,JCI)=CHI(IC,JCI,KC)
C      FORMAT(5X,10E10.2)
C      CONTINUE
C
C      KC IS THE NO. OF LEVELS PRINTED...HERE CONTROLS WHICH
C      LEVELS ARE CONTOURED.
C      IF (KC.EQ.1) CALL DRAW(CPLOT,10,17)
C      CONTINUE
C      WRITE(6,1)
C      GO TO 1600
C
C 1590 FORMAT(95H PUFF POSITION PLOT AND GRID CONCENTRATION PRINTING AR
C 1595 WRITE(6,1590)
C
C 1600 CONTINUE
C      END OF GRID CONCENTRATION PRINTING SECTION
C

```

PUF09360  
 PUF09380  
 PUF09390  
 PUF09410  
 PUF09420  
 PUF09430  
 PUF09440  
 PUF09450  
 PUF09460  
 PUF09470  
 PUF09480  
 PUF09490  
 PUF09500  
 PUF09510  
 PUF09520  
 PUF09530  
 PUF09540  
 PUF09550  
 PUF09560  
 PUF09570  
 PUF09580  
 PUF09590  
 PUF09600  
 PUF09610  
 PUF09620  
 PUF09630  
 PUF09640  
 PUF09650  
 PUF09670  
 PUF09680

PUF09690  
 PUF09710  
 PUF09720  
 PUF09730  
 PUF09750  
 PUF09760  
 PUF09770  
 PUF09780  
 PUF09790  
 PUF09800  
 PUF09830  
 PUF09840  
 PUF09870





PUF10410  
PUF10420  
PUF10430  
PUF10440  
PUF10450  
PUF10460  
PUF10470  
PUF10480  
PUF10490  
PUF10500  
PUF10510  
PUF10520  
PUF10530  
PUF10540  
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PUF10560

PUF10570  
PUF10580  
PUF10590  
PUF10600  
PUF10610  
PUF10620  
PUF10630  
PUF10640  
PUF10650  
PUF10660  
PUF10670  
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PUF10690  
PUF10700  
PUF10710  
PUF10720  
PUF10730  
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PUF10750  
PUF10760  
PUF10770  
PUF10780  
PUF10790  
PUF10800

PUF10810  
PUF10820  
PUF10830  
PUF10840  
PUF10850  
PUF10860  
PUF10870  
PUF10880  
PUF10890  
PUF10900  
PUF10910

```

8930 WRITE(6,1140)
8940 GO TO 9999
8940 NRM1 = NRSTAB - 1
8940 WRITE(6,1030) NRM1
8950 GO TO 9999
8950 WRITE(6,1025) NRSTAB
8970 GO TO 9999
8970 WRITE(6,1015) WINDAV,NTADV
8980 GO TO 9999
8980 WRITE(6,1010) TAU,NTADV
8990 GO TO 9999
8990 WRITE(6,1005)
9000 GO TO 9999
9000 WRITE(6,1000) I
C 9999 CONTINUE
    CALL EFRAME
    STOP
    END

```

CCCCC

SUBROUTINE SIGRIS(HGN,SIGXY,SIGZ)  
THE SUBROUTINE "SIGRIS" (SIGMA-RISE) CALCULATES THE INCREMENT  
IN SIGMA-XY AND SIGMA-Z DURING EACH BASIC ADVECTION STEP.  
FURTHER, THE SUBROUTINE ESTIMATES PLUMERISE ASSOCIATED WITH  
BOUYANCY IN THE EFFLUXES.

FOR Z-COORDINATES OF PUFFS: HEIGHT , GRID UNITS(N) : HGN

COMMON HEATFX(25), I2, DMS, POINT, INTENS(14), STABPA, FBFLX

1, UNN, CONST1, DELZ

INTEG FR POINT

REAL INTENS

CALCULATING GROWTH RATES FOR SIGMAS; DSIGDS

DEFINING EXPERIMENTAL FITTING CONSTANT: FITCST

FITCST = 2.0

DSIGDS = DSIGDS \* FITCST

DSIGDS = DSIGDS \* DMS

SIGZ = SIGZ + DSIGDS \* DMS

CALCULATING PLUME-RISE INCREMENT:

CC

CC



```

      RETURN
1  IF (ITENFT.NE.1) GO TO 2
   WRITE(6,20) INR
      RETURN
2  IF (ITENFT.NE.2) GO TO 3
   WRITE(6,30) INR
      RETURN
3  IF (ITENFT.NE.3) GO TO 4
   WRITE(6,40) INR
      RETURN
4  IF (ITENFT.NE.4) GO TO 5
   WRITE(6,50) INR
      RETURN
5  IF (ITENFT.NE.5) GO TO 6
   WRITE(6,60) INR
      RETURN
6  IF (ITENFT.NE.6) GO TO 7
   WRITE(6,70) INR
      RETURN
7  IF (ITENFT.NE.7) GO TO 8
   WRITE(6,80) INR
      RETURN
8  IF (ITENFT.NE.8) GO TO 9
   WRITE(6,90) INR
      RETURN
9  IF (ITENFT.NE.9) GO TO 1000
   WRITE(6,100) INR
1000 RETURN
      END

```

SUBROUTINE DRAW (A,M,N)

THIS SUBROUTINE CONVERTS THE GRID CONCENTRATIONS TO LOG VALUES  
THEN SMOOTHES AND CONTOURES THE PUFF ARRAY...

DIMENSION A(M,N)

A IS THE ARRAY TO BE SMOOTHED AND CONTOURED  
M,N IS THE DIMENSION OF ARRAY A

```

DO 1553 JC=1,N
JJC=N-JC
JC1=JJC+1
DO 1554 IC=1,M
IF (A(IC,JJC).LT. 1E-12) A(IC,JC1)=0.0
A(IC,JC1)=A(IC,JJC)*1.E13

```

CC  
CC  
CC  
CC  
CC  
CC

PUF11740

PUF11430  
PUF11440  
PUF11450  
PUF11460  
PUF11470  
PUF11480  
PUF11490  
PUF11500  
PUF11510  
PUF11520  
PUF11530  
PUF11540  
PUF11550  
PUF11560  
PUF11570  
PUF11580  
PUF11590  
PUF11600  
PUF11610  
PUF11620  
PUF11630  
PUF11640  
PUF11650  
PUF11660  
PUF11670  
PUF11680  
PUF11690  
PUF11700  
PUF11710  
PUF11720

```

1554 IF(A(IC,JCL).EQ.0.0) GO TO 1554
1555 A(IC,JCL)=ALOG10(A(IC,JCL))
C CONTINUE
1553 WRITE(6,1555) (A(IC,JCL),IC=1,M)
1555 FORMAT(5X,10E10.2)
SMOOTH ARRAY
MM1=M-1
NM1=N-1
DO 200 J=1,N
TEMP=A(I,J)
DO 100 I=2,MM1
TEMP1=A(I,I,J)
A(I,J)=.20*(TEMP+3.*TEMP1+A(I+1,J))
TEMP=TEMP1
100 CONTINUE
200 CONTINUE
DO 400 I=1,M
TEMP=A(I,1)
DO 300 J=2,NM1
TEMP1=A(I,I,J)
A(I,J)=.20*(TEMP+3.*TEMP1+A(I,J+1))
TEMP=TEMP1
300 CONTINUE
400 CONTINUE
DO 1559 J=1,17 (A(I,J),I=1,10)
1559 WRITE(6,1555) (A(I,J),I=1,10)
CALL SET(.1,31,2,58,0,1,0,1,1)
CALL CONREC(A,10,10,17,0,0,1,0,1,1,0)
CALL TICK4(5,8,5,8)
CALL PERIM(9,0,16,0)
CALL FRAME
CALL RETURN
END

```

CCCC CCCCCC

PUF11750

PUF11760  
PUF11770  
PUF11780  
PUF11790  
PUF11800  
PUF11810  
PUF11820  
PUF11830  
PUF11840  
PUF11850  
PUF11860

SUBROUTINE RSPACE(ITENFT,RNR)  
THIS SUBROUTINE HAS THE SAME PURPOSE FOR REAL FIGURES, AS  
ISPACE HAS FOR INTEGER FIGURES.  
RNR : REAL NUMBER TO BE PRINTED.

```

10 FORMAT(1H+,19X,F6.1)
20 FORMAT(1H+,29X,F6.1)
30 FORMAT(1H+,39X,F6.1)
40 FORMAT(1H+,49X,F6.1)

```

PUF11870  
 PUF11880  
 PUF11890  
 PUF11900  
 PUF11910  
 PUF11920  
 PUF11930  
 PUF11940  
 PUF11950  
 PUF11960  
 PUF11970  
 PUF11980  
 PUF11990  
 PUF12000  
 PUF12010  
 PUF12020  
 PUF12030  
 PUF12040  
 PUF12050  
 PUF12060  
 PUF12070  
 PUF12080  
 PUF12090  
 PUF12100  
 PUF12110  
 PUF12120  
 PUF12130  
 PUF12140  
 PUF12150  
 PUF12160  
 PUF12170  
 PUF12180  
 PUF12190  
 PUF12200  
 PUF12210  
 PUF12220  
 PUF12230  
 PUF12240  
 PUF12250

50 FORMAT(IH+,59X,F6.1)  
 60 FORMAT(IH+,69X,F6.1)  
 70 FORMAT(IH+,79X,F6.1)  
 80 FORMAT(IH+,89X,F6.1)  
 90 FORMAT(IH+,99X,F6.1)  
 100 FORMAT(IH+,109X,F6.1)

C

IF(IITENFT.NE.0) GO TO 1  
 WRITE(6,10) RNR  
 RETURN  
 1 IF(IITENFT.NE.1) GO TO 2  
 RETURN  
 2 IF(IITENFT.NE.2) GO TO 3  
 WRITE(6,30) RNR  
 RETURN  
 3 IF(IITENFT.NE.3) GO TO 4  
 WRITE(6,40) RNR  
 RETURN  
 4 IF(IITENFT.NE.4) GO TO 5  
 WRITE(6,50) RNR  
 RETURN  
 5 IF(IITENFT.NE.5) GO TO 6  
 WRITE(6,60) RNR  
 RETURN  
 6 IF(IITENFT.NE.6) GO TO 7  
 WRITE(6,70) RNR  
 RETURN  
 7 IF(IITENFT.NE.7) GO TO 8  
 WRITE(6,80) RNR  
 RETURN  
 8 IF(IITENFT.NE.8) GO TO 9  
 WRITE(6,90) RNR  
 RETURN  
 9 IF(IITENFT.NE.9) GO TO 1000  
 WRITE(6,10) RNR  
 1000 RETURN

//GO.F01F001 DD \* 17 4 1  
 12 3600 0 10  
 3600 40 90  
 PRIMDATA SEPT 29 81  
 217.50 435.00 40.00 1.000E-13 1.0000  
 YES  
 YES  
 YES

```

INST
//GO.FT02F001 DD UNIT=SYSOA,DISP=(OLD,DELETE),DSN=&FT02
//GO.FT03F001 DD *
STABILITY-DATA, SEPT 29 81
1.0000
80.00
//GO.FT04F001 DD *
INDIVIDUAL SOURCE DATA
#01# 1 2 0 0 3600 6.04 15.07 4.0
//GO.SYSIN DD *
INTENSITY-DATA, SEPT 29 81
# 5#
.2500.1000.0500.0100.0300

```

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